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All-painting process to produce respiration sensor using humidity-sensitive nanoparticle film and graphite trace

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KEYWORDS

All-painting process, health monitoring, respiration sensor, nanoparticle film, humidity

ABSTRACT

We propose an all-painting process to produce a respiration sensor made from a humiditysensitive nanoparticle (NP) film and a graphite trace. The sensor is fabricated under ambient air with a simple vacuum-free process for green electronics: solely hand-painting on a cellulose acetate film. A humidity-sensitive silica NP film is painted by brush on pencil-trace graphite electrodes. An all-painted humidity sensor using this film shows 10^6 % sensitivity within a 10-93% humidity change. The film is flexible and the humidity sensor operates as a respiration sensor after bending test. We design an all-painted respiration sensor using the humidity sensor and a painted resistor. Finally, we integrate the all-painted respiration sensor, a flexible temperature sensor, and a portable data logger as a portable bifunctional healthcare device. The device on a mask can monitor human respiration rate and exhaled air temperature simultaneously.

Importance of healthcare devices has been increasing rapidly in modern life. Health monitoring and fitness tracking of vital signs are demands to use healthcare devices $1-3$. Continuous monitoring of vital signs is helpful for early detection of symptoms and disease. In hospital, vital signs of patients are automatically monitored by a bedside monitor with electrical wires to body. Vital signs during fitness and sports activities are usable to assess performance of exercises. A heart rate monitoring system has already been installed in commercial fitness trackers⁴ and the data are collected via wireless communication into smartphones. Recently, monitoring multiple physiological signals by using a single multifunctional device is intensively studied $5-9$.

Respiration rate is one of the vital signs and directly relates to the condition of respiratory organs. In order to detect respiration rate remotely, several types of portable respiration sensors have been proposed^{10–17}. Colloidal nanomaterial films are promising as a humidity-sensitive film to detect respiration^{18,19}. Non-heat resistant polymer films can be in use as a substrate when solution processes to deposit colloidal nanomaterials are carried out at low temperature (< 100 °C). Paper (cellulose) is an attracting green material as a platform of electrical devices because of low cost, lightweight, environmental friendliness, and availability of printing processes^{20–22}. Various electrical devices have been developed on a paper²⁰: field-effect transistors^{23,24}, capacitive touch pads²⁵, memories^{26,27}, and sensors^{28–33}. On a paper, conductive graphite is easily deposited as a pencil trace. The advantages of graphite trace are light, robust, and stable against chemical corrosion²¹. Electrical circuits on paper are easily drawn and modified as compared to conventional lithography and metal deposition processes. Flexible electrical devices using a pencil trace are reported in recent literatures^{28,33–35}. Zhao et al. demonstrated a humidity sensor with drawn graphite and multi-walled carbon nanotube layers.³⁴ They patterned outlines of graphite interdigitated electrodes by printing with AutoCAD. Zhang et al. draw graphite on Ag-Pd interdigitated electrodes to form a simple humidity sensor.³⁵ Kanaparthi showed a pair of graphite electrodes on a paper worked as a capacitive respiration sensor. The sensor on a textile mask monitored human respiration although a numerical derivation of the signal was required to find respiration rates.

Inspired by these works, we propose a simple sensor fabrication process: painting a respiration sensor with a humidity-sensitive nanoparticle (NP) film and graphite trace. Allprinted devices are usually fabricated by using inkjet and screen printers^{27,36,37}. In this study, we define an "all-painted" sensor fabricated solely by hand-painting. Fabrication of all-painted sensors is simple and vacuum free without any electronic facilities. Low-cost and non-toxic green materials such as silica $(SiO₂)$ NP and graphite are used for this process. For electrical interconnection, we use graphite trace as a contact electrode in this work. A $SiO₂ NP film$, which is a humidity sensitive film, is painted on the electrodes by a brush with a colloidal NP solution^{16,38,39}. A fabricated device works as a humidity sensor. We characterize the humiditysensing capability and the sensor. We design an all-painted resistor for fabricating a respiration sensor as well. By implementing an all-painted respiration sensor and a flexible thermistor on a mask, a portable bifunctional healthcare device is produced. The healthcare device can observe respiration rate and exhaled air temperature of a subject. The respiration sensor shows clear respiration signals with high signal-to-noise ratio without baseline drifting.

EXPERIMENTAL SECTION

Fabrication of all-painted sensor. The process for the fabrication of a SiO₂ NP sensor by painting is schematically shown in Figure 1(a). As a flexible substrate, we adopted a singleside mending tape (3M, Scotch Magic Tape) based on a cellulose acetate film. The surface of the tape was matte finished and this tape had a write-on capability by a pencil. A cellulose paper such as a photocopying paper also worked as a substrate. However, the response of a sensor on a photocopying paper was much slower than that on a cellulose acetate film as discussed later. Graphite electrodes were deposited on the tape by using a mechanical pencil with a HB pencil lead and a metal mask. The metal mask had patterns of electrodes (5 mm square) and 200 μm spacing. Sheet resistance of graphite electrodes was 50-100 kΩ/sq. and did not change by exposure to respiration. The sheet resistance does not largely affect the sensor output because the resistance of a SiO2 NP film is much larger as shown later. Zhao et al. reported that the square resistance of graphite electrodes decreased as the graphite content of pencil leads increased.³⁴ A colloidal solution of $SiO₂$ NPs (Nissan Chemical Industries Ltd., ST-XS) was deposited by using a brush between the graphite electrodes and dried at room temperature. A deposited solution was kept on a top of the acetate film and a NP film was gradually formed. The whole fabrication processes were carried out under ambient air. It should be noted that a NP film covered with a cellulose acetate tape did not respond to humidity change: thus the surface-covered NP film worked as a resistor.

Figure 1(b) shows a photo of an all-painted film and an optical microscopy image. Although the NP film is cracked, the resistance of the film responds to humidity change as shown later: therefore, the cracked area is also covered with thin NP layers. Figure $1(c)-(e)$ show atomic force microscopy (AFMWorkshop, TT-2) images of an acetate film, a graphite electrode, and a $SiO₂$ NP film (un-cracked area). Height gradient curves are also shown in Figure 1(f). On a graphite electrode, step structures possibly due to graphite flakes are observed (Figure 1(d)). Surface of a $SiO₂$ NP film is flatter than that of a bare acetate film, which indicates that NPs are densely packed⁴⁰. The thickness of the NP film is approximately 400 nm from line profiles in Figure S1. The scanning electron microscope image of a NP film and a graphite electrode is shown in Figure S1(d). Fabricated all-painted sensors on a 25 μm-thick polyimide film are flexible and can be wrapped around a pen with 8 mm diameter as shown in Figure $1(g)$.

Measurement setup. The humidity-sensing property of an all-painted sensor was measured in a homemade box or a closed vessel with saturated salt solutions. Relative humidity (RH) in the box was controlled by N_2 carrier gas with bubbling distilled water. In case of a closed vessel with saturated salt, relative humidity conditions of 33, 67, 84, 93 %RH were obtained by using saturated solutions of MgCl2, CuCl2, KCl, and KNO3, respectively. Current through the film was measured by a source measure unit (Keithley, 236). RH in the box was simultaneously recorded by using a commercial humidity sensor (TDK, CHS-UGS). The accuracy of the commercial sensor was \pm 5 % of RH. Impedance spectroscopy was carried out by using an LCR meter (NF Corporation, ZM2376). Frequency of AC voltage was changed from 1 Hz to 1 MHz.

For evaluating dynamic response of resistance of SiO₂ NP films, we used a saturated KCl solution in a closed vessel which had $84\% RH^{41,42}$. We monitored resistance of the films while taking the sensor into and out of the vessel. The measurements were carried out in room temperature and 30 % RH. We evaluated response and recovery time by observing current intensity to humidity change. Bending tests of painted sensors were carried out by using a Vernier caliper. Radius of curvature (*r*) was changed from 10 to 1.3 mm. We made bending cycle tests up to 500 times.

Fabrication of bifunctional healthcare device. We integrate an all-painted respiration sensor, a flexible thermistor (SEMITEC, 103JT-025-A; resistance of thermistor $R_T = 9.67 \text{ k}\Omega$; response time ~5 s), and a portable data logger (MbientLab, MetaWearC) into a portable bifunctional healthcare device. A load resistor for reading a voltage change was also painted by using the method in Figure 1(a). We introduced a thermistor to estimate exhaled air temperature and a temperature in air (when no exhaled air is given). Evaluation of exhaled air temperature has been suggested as a non-invasive method in human physiology and clinical researches.43 We made the devices electrically contacted with a silver epoxy paste and a polyurethane wire. The devices were mounted on a 125-μm thick polyimide film for stable measurements. The healthcare device was attached on a medical oxygen mask with a singleside tape. The subject wearing the device recorded their respiration rate and exhaled air temperature simultaneously. The data were collected by using an Android API for MetaWearC in a tablet under 26-28 °C. Respiration rate was calculated by counting the number of respiration in every 30 s.

Figure 1. (a) Schematic illustration of fabrication of an all-painted sensor. Inset photo shows a colloidal solution of $SiO₂$ NPs. (b) Whole picture and optical microscope image of an all-painted film. (c-e) AFM images of (c) acetate film, (d) graphite electrode, and (e) SiO2 NP film, respectively. (f) Height profiles in (c), (d), and (e). (g) Picture of an allpainted device wrapped around a pen (diameter: 8 mm).

RESULTS AND DISCUSSION

Humidity dependence of all-painted device. A deposited SiO₂ NP film works as a humidity-sensitive film; and thus, the device works as a humidity sensor. Figure 2(a) shows current versus voltage characteristics of an all-painted humidity sensor in various RH. Under \leq 10 % RH, no current larger than base noise (\sim 50 pA) is observed because the SiO₂ NP film is insulator. Current intensity due to proton transport increases as RH increases because water molecular layers are formed on a surface of the NP film^{44–46}. Note that current intensity without a NP film is 30 times smaller than that with a NP film at 40 % RH (Figure S2). Resistance of a painted SiO2 NP film versus RH is shown in Figure 2(b). Resistance changes by four orders of magnitude from 10 to 80 %RH due to proton transport on insulator, which is similar to the case of a drop-coated SiO₂ NP film¹⁶. The resistance is more than 10 M Ω and much larger than the resistance of the graphite electrodes. A Cole-Cole plot of a NP film at 84 % RH is shown in Figure 2(c). From 100 Hz to 1 MHz, the plot shows a semicircle due to an equivalent parallel circuit of a resistance of a NP film (30 MΩ) and a parasitic capacitance (3.3 pF)^{47,48}. On the contrary, a diffusion effect of protons appears in the frequency lower than 100 Hz and the impedance slightly increases as the frequency decreases (Warburg impedance)^{38,48,49}. Figure S3(a) shows Bode plots of impedance magnitude. Equivalent circuits in 18 and 84 % RH from impedance spectroscopy are shown in Figure S3(b). In the Supporting Information (Figure S4 (a-d)), the Cole-Cole plots of another NP film in different RH are shown. After exposure to 93 % RH, the current-voltage characteristics do not degrade (Figure S4(e)). Thus, this NP film can be in use for detecting human breath which has almost 100 % RH.

Figure 2. (a) Current versus voltage characteristics of an all-painted humidity sensor in various RH. (b) Resistance of an all-painted humidity sensor as a function of RH. Open and filled marks represent measurements increasing and decreasing humidity, respectively. (c) Cole-Cole plot of a painted SiO2 NP film. Frequency changes from 1 Hz to 1 MHz. All of the measurements were used in a homemade box.

To prove the concept to fabricate a NP film sensor by all-painting processes, we fabricate 15 humidity sensors as shown in Figure 3(a). All the sensors show similar current-voltage curves (Figure S5(a)). The resistance response to dynamic humidity change between 30 and 84 % RH is shown in Figure 3(b). Figure 3(c) shows the variation of the sensor resistance. The average resistances at 30 % and 84 % RH are 1.4 GΩ and 34 MΩ, respectively. Response time and recovery time are defined as the time to achieve 90% of total change. The response time and recovery time of all-painted sensors are evaluated to be 31.4 and 6.5 s, respectively (Figure S5(b)).

It is noted that the response is sufficient enough to detect human respiration $(\sim 0.2 \text{ Hz})$ because we use a dynamic output to humidity change. A current change of 10 % of total change is detectable and the average time to achieve 10 % of total change of current are 4.8 (rise) and 0.7 (fall) s, respectively (Figure S5(c) and (d)). Therefore, we do not need to use a saturated signal of the humidity sensor in this application. It is possible to calculate human breathing rates by counting the number of peaks of the dynamic output as shown later.

A possible method to decrease the response/recovery time is to reduce the thickness of the 400-nm SiO₂ NP film. According to Miao et al.⁵⁰, water absorption capacity of a thinner humidity-sensitive film might result in short response/recovery time. Another possible method is to reduce the gap between graphite electrodes. However, it is difficult to prepare a shorter gap than 200 μm by pencil drawing and we cannot examine the gap size dependence. Table 1 shows statistical values of sensor properties. We do not have a clear reason why the recovery time is shorter than the response time.

	Resistance $\sqrt{\text{in } 84\% \text{RH}}$	Lable 1. Diamstical values of selisof properties Resistance in 30 %RH	Rise time	Fall time
Average	$34\ \mathrm{M}\Omega$	$1.4\ \mathrm{G}\Omega$	4.8 s	0.7 s
Standard deviation	$20 \text{ M}\Omega$	$0.97~\text{G}\Omega$	1.7 s	0.4 s

Table 1. Statistical values of sensor properties

We discuss an appropriate substrate for all-painted humidity sensors. We can fabricate an all-painted humidity sensor on a photocopying cellulose paper. However, a painted NP film on a photocopying cellulose paper shows much slower response (response/recovery time: 535/86.8 s, Figure S6). When a colloidal solution is deposited on a photocopying paper, SiO2 NPs are dispersed inside the paper and the whole paper becomes a humidity-sensitive film. Because water molecules are trapped on SiO₂ NPs inside the paper, response and recovery of the sensor become slow. This result indicates that a substrate for all-painted humidity sensors needs water-resistance and does not absorb colloidal solution.

Figure 3. (a) Picture of 15 painted humidity sensors. Sample IDs are shown in the picture. Acetate films are attached on a polyimide film (125 μm thickness). (b) Dynamic response of resistance of painted films by changing humidity. 10 V is applied as a bias voltage. (c) Resistance distribution of painted films in 84 % and 30 % RH.

Bending cycle test. Figure 4(a) shows a resistance of an all-painted NP humidity sensor as a function of bending radius of curvature. Resistance does not largely change even in the radius of curvature (*r*) of 1.3 mm. Fluctuation of the resistance may be due to change of a current path through the bent SiO2 NP film. As the number of bending cycles increases, the resistance increases as shown in Figure $4(b)$ because the SiO₂ NP film is possibly damaged by bending. However, even after 500 times bending tests in *r*=1.3 mm, the sensor detects exhaled air from nose (distance from the sensor: \sim 10 cm). Figure 4(c) and 4(d) show responses of the sensor to exhaled air before and after 500 bending cycles, respectively. Five successive respiration can be detected after the bending cycle test. The fluctuation of the current intensity under exhaled air is due to the fluctuation of human respiration because the amount of exhaled air and the rate are not precisely controlled. The results in Figure 4 indicate that the all-painted SiO2 NP sensor has high flexibility.

Table 2 summarizes recent literature reporting humidity sensors on cellulose. Despite the simple and easy fabrication process, the sensitivity $(10^6 \text{ % between } 10\text{-}93 \text{ %RH})$ and response/recovery time (31.4 s/6.5 s) of the all-painted sensor are as good as those of the previous reported paper-based humidity sensors. Table 2 also includes recent literature on ultrafast response and flexible polymer humidity sensors. Compared to these sensors, an advantage of the all-painted sensor is the easiness of the fabrication process, which does not require any electrical facilities, such as printing and vacuum evaporation facilities. It is beneficial if human respiration is monitored by using the all-painted humidity sensor produced on site.

Figure 4. (a-b) Resistance of an all-painted humidity sensor as a function of (a) radius of curvature and (b) bending cycles in *r*=1.3 mm. (c-d) Response to exhaled air (c) before and (d) after the bending test. Current under bending in $r=1.3$ mm is also shown in (c). Dashed rectangles indicate that the current intensity under no exhaled air.

Table 2. Properties of humidity sensors on cellulose in recent literature. NA: No data. Properties of ultrafast response and flexible polymer humidity sensors are also shown for comparison.

All-painted resistor with SiO2 NP film. In order to fabricate a portable respiration sensor, we design an electrical circuit in Figure 5(a). The circuit consists of a humidity sensor (R_R) and a resistor (*R*L) which are solely fabricated by painting. A bias voltage from a button buttery is applied to a series of R_R and R_L , and then an output voltage V_{out} in R_L is monitored. The output voltage in Figure 5(a) is changed by large R_R change when R_R is exposed to exhaled air.

It should be stressed here that we also fabricate a resistor (a humidity-insensitive element) by painting. A resistor is fabricated by covering a SiO2 NP film with an acetate tape (Figure 5(b)). Although the current-voltage curve does not largely change with covering the surface (Figure 5(c)), the resistance becomes independent on humidity as shown in Figure 5(d). This indicates a surface-covered NP film is protected by the tape from adsorption of water molecules. With assembling all-painted resistor and humidity sensor, we can demonstrate an all-painted respiration sensor as follows.

Figure 5. (a) Electrical circuit of an all-painted respiration sensor. *RR* and *RL* represent a humidity sensor with a bare $SiO₂ NP film$ and a resistor with a surface-covered $SiO₂ NP film$, respectively. (b) Photos of bare and surface-covered SiO2 NP films. (c) Current-voltage curves and (d) current response to humidity change of the $SiO₂ NP films$. Colored region in (d) indicates that the films are in 84 % RH. A bias voltage (10 V) is applied to each device in (d).

Bifunctional monitoring of respiration and exhaled air temperature. Figure 6(a) shows a sensor structure for a portable bifunctional healthcare device. Figure 6(b) shows a sensor response to a finger proximity within 2 mm. Water evaporation from a fingertip is clearly monitored as increase of the output voltage (Figure $S7(a)$ and $S7(b)$). Figure $6(c)$ is a picture of an attached healthcare device on a medical oxygen mask. The device is placed near ventilation holes of the oxygen mask. A portable data logger is also attached on a mask with a single-side tape. Figure 6(d) shows response of the healthcare device to three deep respiration of a subject at rest. The device detects respiration and exhaled air temperature (\sim 35 °C) from the subject (body temperature: \sim 36 °C). Exhaled air temperature is lower than body temperature by \sim 1°C. Humidity in the exhaled breath is almost saturated (\sim 100 %) because breath air is humidified by human respiratory systems. 2.3 V of the response corresponds to 100 % RH in this study. It should be noted that the all-printed respiration sensor can follow various respiration patterns (up to 40 min⁻¹) such as apnea, hyperpnoea, and dyspnea (Figure S7(c)). The sensor signals are clear with high S/N ratio (-23) without baseline drifting.

Figure 6(e) shows respiration and temperature of exhaled air during walk and run. The sensor fully tracks an increase of respiration rate $(14 \text{ min}^{-1} \text{ to } 20 \text{ min}^{-1})$ by running. Because the output of the temperature sensor clearly corresponds to that of the all-painted NP respiration sensor, we prove the all-painted respiration sensor works correctly. However, the temperature sensor does not fully follow the exhaled air temperature in this measurement because of the slow response. Because graphite and $SiO₂ NP$ are robust and chemically stable, the sensor can be stored in ambient air more than 20 days (Figure S7(d)). The breathing patterns of "Walk", "Run" and "Rest" in Figure 6(e) is shown in the Supporting Information (Figure S7). The shape of the signals is almost identical. We checked that volatile organic compounds (VOCs) in exhaled gas do not have influence in the sensor output (Figure S9). This portable bifunctional

respiration sensor has a large impact for many fields such as extreme sports, early finding of disease, and physiological evaluation $14,19$.

Figure 6. (a) Prototype of a portable healthcare device using an all-painted respiration sensor and a flexible temperature sensor. (b) Response of the device to finger proximity (2 mm away). Shadowed regions correspond to the time in a finger proximity. (c) Attached healthcare device on a medical oxygen mask. (d) Response to deep respiration. (e) Demonstration of successive monitoring of respiration rate and exhaled air temperature in exercise.

CONCLUSIONS

We have developed an all-painting process to produce a sensitive respiration sensor by using solely hand-painting. The sensor was prepared with a brush-painted humidity-sensitive NP film and graphite traces, which were low-cost and non-toxic green materials. We first demonstrated an all-painted humidity sensor on an acetate film. Reproducible fabrication was achieved and the sensitivity and the response/recovery time of the humidity sensor were $10⁴$ and 31.4 s/6.5 s, respectively. The humidity sensor was flexible and operated normally after 500 bending cycles in *r*=1.3 mm. We designed an all-painted respiration sensor comprising the humidity sensor and a painted resistor. We integrated the all-painted respiration sensor, a thermistor, and a portable data logger as a portable bifunctional healthcare device. The healthcare device simultaneously tracked human respiration rate and exhaled air temperature. Painting is a simple, easy, and green process to produce healthcare devices for social demands without electrical facilities.

ASSOCIATED CONTENT

Supporting information

The Supporting Information is available free of charge on the ACS Publications website at DOI:***. AFM images, profiles, and a SEM image of a SiO2 NP film; Current-voltage curves of graphite electrodes without a NP film; Bode plots of a NP film; Cole-Cole plots in different relative humidity; Characteristics of 15 all-painted sensors; Characteristics of all-painted sensor on a photocopying paper; Detection of water evaporation from a fingertip and various rates of respiration patterns; each breathing pattern of Figure 6(e); VOC gas exposure test.

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Notes

The authors declare no competing financial interest. The research has been approved by the institutional review board in Kobe University.

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Table of Contents Graphics

SYNOPSIS: We propose an all-painted fabrication process of a respiration sensor based on a humidity-sensitive silica nanoparticle film and graphite trace.