



Detection of Hemodynamic Characteristics Before Growth in Growing Cerebral Aneurysms by Analyzing Time-of-Flight Magnetic Resonance Angiography Images Alone: Preliminary Results

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1 Title: Detection of Hemodynamic Characteristics Before Growth in Growing Cerebral Aneurysms
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3 - Preliminary results -

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8 growing, enlargement

1 ABSTRACT

2 Objective: Cerebral aneurysm growth often precedes rupture. Definite contributors to aneurysm
3 growth have not been determined even by means of recently developed commercially available
4 computational fluid dynamics (CFD) software. We developed an original CFD tool that can
5 analyze data from time-of-flight magnetic resonance angiography (TOF-MRA) prior to growth in
6 the growing aneurysms and investigate possible factors for aneurysm growth in the near future.

7 Methods: We retrospectively reviewed unruptured aneurysms that were treated at our institute
8 because of aneurysm growth (growing group) between April 2013 and March 2017. Stable
9 aneurysms that had demonstrated no growth for more than five years were selected (stable group).
10 TOF-MRA data of these aneurysms were retrospectively converted to three-dimensional vessel
11 geometric data; three hemodynamic indices including streamline, wall shear stress (WSS), and
12 oscillatory shear index were calculated by our original CFD tool using the lattice Boltzmann
13 method to quantitatively compare the two groups.

14 Results: Six growing aneurysms and 6 stable aneurysms were analyzed. Of the 6 growing
15 aneurysms, WSS on the focal aneurysmal sac increased temporally in the vicinity of the constant
16 low WSS area at the peak systolic phase. By contrast, WSS did not increase during any part of the

- 1 cardiac cycle in three of the six stable aneurysms. The peak values of WSS were significantly
- 2 different between the two groups.
- 3 Conclusion: A focal increase in WSS in the peak systolic phase may be a risk factor for
- 4 aneurysm enlargement in the near future.

1 INTRODUCTION

2 Unruptured intracranial aneurysms are mostly asymptomatic. A few per year enlarge and later
3 rupture, causing subarachnoid hemorrhage (SAH)^{1, 2}. Despite substantial improvements in clinical
4 care of these patients, the morbidity and mortality of aneurysmal SAH remain too high to be
5 ignored, and some patients suffer devastating outcomes³. Therefore, an objective assessment tool
6 that would reliably identify patients at risk for aneurysm growth and rupture would be beneficial,
7 enabling preventative interventions, such as endovascular coiling and microsurgical clipping².

8 Some clinical and morphological factors, including patient sex and aneurysm size and location,
9 may help predicting the rupture risk of incidentally detected aneurysms^{1, 4, 5}. However, the
10 trustworthiness of patient specific factors in prediction of aneurysm rupture remains unclear.

11 Recent advances in computational fluid dynamics (CFD) have enabled the study of
12 hemodynamics in realistic aneurysm geometries⁶. Among hemodynamic parameters, wall shear
13 stress (WSS) was reported to be a key parameter in the development, growth, and rupture of
14 intracranial aneurysms^{7, 8}. Despite a variety of efforts to study this matter, researches on its
15 relationship with the risk of aneurysm growth and rupture showed conflicting results: in some
16 studies this risk was associated with high WSS, while in others with low WSS, in an individual

aneurysm⁹⁻¹¹.

In order to clarify hemodynamic features contributing to aneurysm growth and rupture, a retrospective review and analysis of the original cerebral aneurysm data before growth or rupture should be ideally conducted, in order to determine the actual factors causing aneurysm growth and rupture¹². Unfortunately, little data on aneurysms hemodynamic status before growth or rupture are available after they grow or rupture, which made this retrospective analysis almost impossible¹³.

Growing, unruptured intracranial aneurysms have often been detected by time-of-flight-magnetic resonance angiography (TOF-MRA), a widely used magnetic resonance imaging (MRI) sequence used to screen for intracranial abnormalities owing to its non-invasive nature¹⁴. However, no study on CFD analysis of TOF-MRA data has been published, because commercially available CFD software could compute the data from rotational angiography or three-dimensional (3D) computed tomography angiography (CTA), but not from TOF-MRA.

Therefore, we launched and developed a new in-house CFD tool using only TOF-MRA images for analyzing the fluid dynamics of cerebral aneurysms, and named it “AN2WER”, abbreviated from “Aneurysms Answer.”

The objective of the present study was to identify possible factors predicting impending

aneurysm growth using our original CFD tool, AN2WER, by analyzing the flow-dynamic features of growing aneurysms using TOF-MRA data collected before growth and comparing quantitatively obtained data to those of stable aneurysms.

METHODS

Patient population (Table 1)

This was a retrospective study. Between April 2013 and March 2017, a total of 526 patients were referred to our institute with the diagnosis of unruptured intracranial aneurysms, and most of these patients were followed-up with TOF-MRA annually. Among them, 9 aneurysms were found to have grown without symptoms. We enrolled six of those patients as the growing group, according to the following inclusion criteria: 1) saccular aneurysm; 2) age between 20 and 90 years; 3) enlargement by 1.0 mm or more in the longest line originating from the centroid of the neck surface compared to previous TOF-MRA images; 4) at least a six-month interval from the initial images; and 5) available TOF-MRA data on prior-to-growth aneurysm status.

In the same patient population, we searched for stable aneurysms in patients who met the following inclusion criteria: 1) saccular aneurysm; 2) age between 20 and 90 years; 3) no change in the size or shape of the aneurysm for at least five years; and 4) available initial TOF-MRA data.

We randomly selected six stable aneurysms in five patients.

MRI findings of these patients were certified by two radiologists.

Our institutional review board approved this study, and written informed consent was obtained from all patients.

TOF-MRA condition

The three-dimensional TOF-MRA images were acquired on 1.5T or 3.0T MRI scanners (Achieva 1.5T Nova Dual, Philips; Achieva 3.0T TX Quasar Dual, Philips; Ingenia 3.0T R5.1.7, Philips; Taitan 3T, Toshiba Medical Systems). The imaging parameters for 3D TOF-MRA on these four scanners were as follows: field of view: 207 mm×230 mm, 184 mm×230 mm, 184 mm×230 mm and 200 mm×192 mm; matrix: 140×400, 243×608, 243×608 and 208×272; and repetition time/echo time: 25 ms/6.91 ms, 25 ms/3.45 ms, 25 ms/3.45 ms and 21 ms/3.4 ms. The slice thickness was 1.1 mm for the first three scanners and 1.0 mm for the Taitan 3T. The parameters

for each scanner were manufacturer-installed settings and were not customized ones.

CFD analysis with AN2WER

Blood flows were simulated using the lattice Boltzmann method (LBM), which gives the time evolution of the velocity distribution functions, f_i , of the i th group of fluid particles by accounting for particle advection and collision. LBM solves the following lattice Boltzmann equation for the i th discrete velocity distribution function f_i ¹⁵:

$$f_i(\mathbf{x} + \mathbf{c}_i \Delta t, t + \Delta t) = f_i(\mathbf{x}, t) + \Omega_i$$

where \mathbf{x} is the Cartesian coordinate, $\Delta \mathbf{x}$ is the grid size, t is the time, Δt is the time step size, \mathbf{c}_i is the discrete velocity of the i th distribution function, and Ω is the collision operator, which is modeled using the single relaxation time approximation:

$$\Omega_i = -\frac{f_i(\mathbf{x}, t) - f_i^{eq}(\mathbf{x}, t)}{\tau}$$

where the superscript *eq* denotes the equilibrium value, and τ is the relaxation time¹⁵. The macroscopic variables (density and velocity) were obtained by taking moments of f_i . Nineteen discrete velocity components (the D3Q19 discrete velocity model) were used for the 3D simulations.

Cartesian computational grids were used in the lattice Boltzmann simulations, whereas the curved boundaries of blood vessels reconstructed from the aneurysmal geometrical models were accounted for by applying the bounce-back boundary condition. For the reconstruction of the geometrical model, TOF-MR data obtained at 1.5T or 3.0T (Fig. 1A) were imported to OsiriX (Pixmeo, Bernex, Switzerland), which enabled us to obtain a geometrical model represented by a set of triangular elements (stereolithographic (STL) mesh data) (Figs. 1B and C). The interpolated bounce-back rule for curved boundaries¹⁶ was used to address the complicated channel structure of blood vessels. The distance from the boundary was required at each grid point under this bounce-back rule; therefore, the signed-distance function was reconstructed from the STL mesh (Fig. 1D)¹⁷. LBM was suitable for parallel computing owing to the locality of the collision process. The General-Purpose Computing on Graphics Processing Units was employed for parallel computing.

The Reynolds number, Re , and the Womersley number, Wo , were set to typical values in cerebral arteries, i.e., $Re = 200$ and $Wo = 2.5$,¹⁸, where $Re = U_0 D / \nu$, $Wo = \omega D^2 / 4\nu$, U_0 is the mean inlet velocity, D is the circle-area-equivalent inlet diameter, ν is the kinematic viscosity, and ω is the angular frequency of pulsatile blood flow. The unsteady flow rate of blood was given as a simple

function of time to model typical pulsatile flow, (see Fig. 1E, in which U is the time-dependent inlet velocity and T is the period of cardiac cycle)¹⁹. The non-Newtonian characteristics of blood were accounted for by means of the Casson model for viscous stress²⁰. It should be noted, however, that the Bingham number, Bi , in cerebral arteries is typically small, e.g., 0.1, such that the non-Newtonian effect on blood flow is expected to be small. The Bingham number is defined as $Bi = \tau_0 D / \eta U_0$, where τ_0 is the yield stress and η is the viscosity.

With this tool, named “AN2WER”, we could perform patient-specific pulsatile blood flow simulations for the arterial geometry during the cardiac phase and calculated three hemodynamic indices: (a) stream line, (b) WSS, (c) oscillatory shear index (OSI). It should be noted that in the following sections, the viscous shear stresses in evaluation of WSS and OSI were scaled by $\rho U_0^2 / 2$, which is the time-averaged dynamic pressure in a parent artery, to clearly show how large the shear stresses in cerebral aneurysms are compared with the kinetic energy of the blood flow in the parent arteries.

Accuracy of AN2WER compared to that of the conventional tool

To confirm the accuracy of AN2WER, we calculated WSS at the sac and parent artery of each

aneurysm, one by using CTA data after growth with commercially available CFD software Hemoscope Ver. 1.5 (EBM corp., Tokyo, Japan), and another by using TOF-MRA data after growth with AN2WER. These results were compared qualitatively regarding WSS distribution.

Detection of factors contributing to aneurysm growth

Using AN2WER, we performed CFD analysis using TOF-MRA data of the growing and the stable group and calculated streamline, WSS, and OSI. These results were assessed qualitatively by comparing the distribution of color maps between the groups. If differences could be detected in two parameters, including WSS and OSI, quantitative evaluations were performed as described above.

Statistical analysis

Continuous variables were presented as means and standard deviations, and categorical variables were presented as percentages. Welch's *t*-test was used to compare continuous variables and proportions. Fisher's exact test was used to analyze differences in categorical factors. All statistical analyses were performed using EZR (Saitama Medical Center, Jichi Medical University,

Saitama, Japan), a graphical user interface for R 3.0.1 (R Foundation for Statistical Computing, Vienna, Austria). A p value <0.05 was considered statistically significant.

RESULTS

Patient characteristics

In the growing group, there were five women and one man, with a mean age of 63.0 years (range, 45-80 years). Two internal carotid artery (ICA) aneurysms, two anterior communicating artery (Acom) aneurysms, and one aneurysm each of the middle cerebral artery (MCA) and distal anterior cerebral artery were included. The initial maximum aneurysm diameter ranged from 2.5 to 8.5 mm (mean, 4.1 ± 2.0 mm). Aneurysms enlarged to sizes ranging from 4.5 mm to 11.8 mm (mean, 6.1 ± 2.6 mm) over a clinical observation period lasting an average of 44.7 months (Table 1).

In the stable group, by contrast, there were five women and one man with a mean age of 76.3 years (range, 60 to 105 years). Three ICA aneurysms and one aneurysm each of the Acom, the MCA, and the junction of the vertebral artery and the posterior inferior cerebellar artery were included. The maximum aneurysm diameter ranged from 4.1 to 7.0 mm (mean, $5.5 \text{ mm} \pm 1.0 \text{ mm}$).

Aneurysms were stable over an observation period lasting an average of 76.3 months (Table 1). No significant differences were found between the two groups in terms of age, male/female ratio, follow-up period, or initial aneurysm size.

Illustrative case (Fig. 2)

A 69-year-old woman was incidentally found to have an unruptured right IC-posterior communicating artery aneurysm that was 8.5 mm in maximum diameter. The aneurysm gradually enlarged to 11.8 mm after eleven months of clinical observation, and the patient underwent surgical clipping to prevent its rupture.

CFD analysis was retrospectively performed with AN2WER using TOF-MRA images acquired at the initial examination and after aneurysm enlargement. Imaging and analysis of flow dynamics including streamline, WSS, and OSI were successfully obtained; these imaging data included dynamic WSS videos spanning one complete cardiac cycle (Fig. 2). In the peak systolic phase, WSS was increased at the focal aneurysmal sac where the aneurysm would enlarge in the future (Fig. 2).

Accuracy of AN2WER compared to that of the conventional tool

Among a total of six growing aneurysms, four patients underwent surgical interventions, including three microsurgical clippings and one endovascular coiling at our institute. The three patients who underwent clipping had both 3D-CTA and TOF-MRA data recorded after growth. We tried to use TOF-MRA data for analysis with Hemoscope Ver. 1.5. However, it could not read the TOF-MRA data as expected, and the data could not be analyzed. Therefore, we used 3D-CTA data recorded after growth to conduct hemodynamic analysis with Hemoscope Ver. 1.5, and successfully calculated WSS. In addition, we applied AN2WER to TOF-MRA data recorded after growth to calculate WSS and compared the results of hemodynamic analysis with Hemoscope Ver. 1.5 (Fig. 3). The distribution of high and low WSS in all three aneurysm sacs and around the aneurysm necks calculated with Hemoscope Ver. 1.5 was quite similar to the results obtained with AN2WER (Fig. 3).

Detection of factors contributing to aneurysm growth

Imaging and analysis of flow dynamics were successfully obtained in all cases (Figs. 2, 4, 5). In all six growing aneurysms, marked increases in WSS were demonstrated at the focal areas on

the aneurysm sacs in the vicinity of constant low WSS areas, at the peak systolic phase before aneurysm growth. The values for cases 1 to 6 were 0.074, 0.106, 0.37, 0.13, 0.26, and 0.25, respectively (Fig. 4). By contrast, in three of six stable aneurysms (Fig. 5; cases 1, 3, 5), no apparent increase in WSS was recognized at the aneurysm sac. The values were 0.0066, 0.045 and 0.0019, respectively. In the remaining three stable aneurysms (Fig. 5; cases 2, 4, 6), a focal, generally mild, increase in WSS was demonstrated in the peak systolic phase, and the values were 0.487, 0.073 and 0.117, respectively.

The peak WSS values of the growing aneurysms during the peak systolic phase had a median of 0.190 (interquartile range, 0.112 to 0.258), and those of stable aneurysms had a median of 0.045 (interquartile range, 0.007 to 0.073) (Fig. 6). The peak WSS tended to be higher in growing aneurysms than in the stable aneurysms. Among the stable aneurysms, case 2, a paraclinoid aneurysm, had an outlier value of 0.487, much higher than the upper whisker, and was excluded. Finally, these differences were statistically significant ($p < 0.05$) (Fig. 6).

Neither the geometric flow streamline nor the OSI showed any specific differences between growing and stable aneurysms.

1 **DISCUSSION**

2 We successfully performed CFD analysis using TOF-MRA images alone using our newly
3 developed CFD tool AN2WER. This is the first report on successful CFD analysis using TOF-
4 MRI images alone for cerebral aneurysms. The tool enabled us to conduct a retrospective analysis
5 of original aneurysm data before growth and to demonstrate the actual hemodynamic situation
6 before aneurysm growth in growing aneurysms. We found that transient, focal high WSS areas of
7 aneurysm sacs in the vicinity of stable low WSS areas at the peak systolic phase was associated
8 with future aneurysm growth.

9

10 ***Significance of CFD analysis from TOF-MRA***

11 TOF-MRA might not provide accurate geometric information²¹, and its data have been assumed
12 to be unsuitable for CFD analysis. However, TOF-MRA is a less invasive examination method that
13 can be performed without injection of contrast medium or exposure to radiation. Therefore, it is
14 familiar and popular as a follow-up tool for incidental detection of aneurysms and has often revealed
15 growing unruptured intracranial aneurysms. If the data of TOF-MRA could be used for CFD
16 analysis, we could analyze the original flow conditions prior to aneurysm growth.

1 However, commercially available software programs could use only high-resolution images
2 from rotational angiography or CTA, but not from TOF-MRA, and these data are used to solve
3 Navier-Stokes equations by means of finite element techniques or finite volume techniques, and
4 to calculate numerical hemodynamic indices, including WSS and OSI. The resolution of TOF-
5 MRA seemed to have been inferior to that of the former two facilities, possibly explaining why
6 commercially available software could not solve the data of TOF-MRA accurately. Therefore, no
7 reports of CFD analysis for unruptured cerebral aneurysms using data from TOF-MRA alone are
8 currently available. Actually, in the present study, we tried to solve the data of TOF-MRA in three
9 cases using Hemoscope and failed to do so.

10 Phase-contrast MRI (PC-MRI) is known to be a non-invasive sequence that is and able to reveal
11 intracranial arteries and cerebral aneurysms as well as TOF-MRA, which can be performed without
12 contrast medium or exposure to radiation¹⁴. Therefore, there have been a few reports of CFD
13 analysis using PC-MRI^{14, 22, 23}. However, PC-MRI is an unusual sequence because of its time-
14 consuming matter, and it has not been adopted for medical check-up screening for cerebral
15 aneurysms. TOF-MRA has been a unique and widely used sequence for screening of intracranial

cerebral aneurysms because of its less-invasive, time-saving character and because the geometrical information provided by this technique is better than that of PC-MRI.

In this study, we first successfully used TOF-MRA alone in CFD analysis by solving LBM as an alternative to solving Navier-Stokes equations. This method is not yet popular for computational hemodynamics and no commercially-available software that uses the lattice Boltzmann equation to analyze hemodynamics of cerebral aneurysms has been established. Only a few authors have reported their experiences with hemodynamic simulation for cerebral aneurysms by applying the lattice Boltzmann equation using their in-house code^{24, 25}. Their conclusions were that LBM could be considered an alternative solver for computational hemodynamics of cerebral aneurysms. Thus, we tried to solve the data of TOF-MRA with LBM, and we succeeded. LBM appears to be a suitable solver for TOF-MRA data.

It remains uncertain why the LBM could solve the data of TOF-MRA. When operating the Hemoscope, we needed to accurately trace and register the centerline of the target vessels. With the rough images of TOF-MRA, it appeared that Hemoscope could not recognize the centerline precisely. However, with our tool using LBM, we did not need to trace the centerline of the parent arteries. The rough surface of vessels was smoothed appropriately enough with Osirix to to solved.

Although no more than three cases were compared qualitatively, we found that the distribution of WSS on the aneurysm sacs calculated by our in-house CFD analysis tool using LBM was quite similar to that obtained by commercially available software using Navier-Stokes equations. Our tool might become an alternative method for CFD analysis of cerebral aneurysms with the great advantage that it can analyze TOF-MRA data.

Prediction of aneurysm growth

Few previous studies analyzed the hemodynamics of growing intracranial aneurysms using longitudinal data, but they reported confusing and inconsistent results^{9, 12, 26, 27}. Boussel et al. analyzed hemodynamics in seven growing aneurysms and proposed that the growth occurred at regions of abnormally low WSS⁹. Similarly, Brinjikji et al found that growing aneurysms had larger areas under low WSS than did stable aneurysms²⁶. By contrast, Sforza et al. suggested that concentrated high WSS could represent the characteristics of hemodynamic environments that promoted aneurysmal growth²⁸. Others concluded that the growing region could be exposed to either high WSS or low WSS²⁷.

Possible reasons for these inconsistent results might include varying methods of evaluation²⁹.

For example, Boussel et al. evaluated WSS as the time average, not the maximum, during the cardiac cycle and reported that time-averaged WSS was significantly lower in the area of the aneurysm growth⁹. Brinjikji et al. reported that growing aneurysms had significantly greater area under low WSS than did stable aneurysms; their study did not focus on lesions with high WSS²⁶.

We presumed that the problem was not the extent of low WSS. We focused on the time-dependent increase in WSS on the aneurysm sac during the cardiac cycle. We found that aneurysms with even small areas of high WSS that were recognized only at the peak systolic phase could grow in the future, as in cases 2, 4 and 6 (Fig. 4). If WSS was calculated as a time average, this small area of temporally high WSS could disappear into the wide area of low WSS, and we would not detect its existence. In fact, Brinjikji et al. reported similar cases, with a wide area of low WSS and focal high WSS on the aneurysm sac that grew during the 1-year follow-up²⁶. However, this focal high WSS was not the focus of their study. Not only a wide area of low WSS but also an area of temporarily high WSS, though small, might be necessary for aneurysm growth. In this study, we found that the difference in this temporal increase of WSS was statistically significant between growing and stable aneurysms.

Recently, Sforza et al. reported that growing aneurysms tended to have complex intrasaccular

flow patterns that induced non-uniform WSS distributions with areas of concentrated high WSS and large areas of low WSS. Their findings were in agreement with our findings²⁸.

Although aneurysm growth has been found to be highly related to aneurysm rupture, the most important task in the management of unruptured aneurysms is to predict ruptures before they occur as opposed to merely when they grow. This problem is yet to be solved, and the "high WSS or low WSS" issue remains confusing in the literature. In recent published articles, other hemodynamic parameters including WSS gradient, OSI, and aneurysm formation indicator, had been investigated to clarify cerebral aneurysm condition, but had not been fully succeeded^{29, 30, 31}. Our novel CFD tool AN2WER appeared to analyze TOF-MRA data accurately. Using this technique, we will be able to measure these hemodynamic parameters by analyzing TOF-MRA data prior to aneurysm rupture in ruptured aneurysms, and expect to be able to propose risk factors for aneurysm rupture from a new viewpoint.

Limitations

The current study has some limitations. First, as with all CFD studies on cerebral aneurysms, several assumptions were made. Inflow profiles were not patient-specific and were taken from a

cohort of healthy patients. The vessel wall was assumed to be rigid^{32, 33}. However, previous investigators indicated that these are second-order issues with only minimal effects on flow dynamics, whereas the most important factor is the actual vessel geometry^{34, 35}.

Second, the sample size was too small to establish an original CFD tool or to detect undeniable factors. We realize that our results are preliminary. We compared solved results between AN2WER and Hemoscope in no more than three cases. With this limited comparison, a potential error or inaccuracy could not be denied sufficiently in smoothing the anatomical data. We should investigate more cases to clarify the accuracy of AN2WER. Moreover, in the detection of factors contributing to aneurysms growth, we compared only six aneurysms between the two groups. Although we obtained a statistically significant result, we are going to perform further analysis on more cases accumulated retrospectively and to perform prospective observation of analyzed aneurysms to obtain definite results. The problem with this investigation is not only that we have a few chances to encounter the growing aneurysm in the outpatient department, but also its complicated procedure and time-consuming analysis. In order to resolve these matters, we will perform a multicenter study to accumulate more cases, improve AN2WER, and facilitate and save time in analysis. Furthermore, in terms of small sample size, Case 2 in the stable aneurysm group,

1 which was the only case harboring a paraclinoid aneurysm, was excluded for having an outlier
2 value. We presumed this outlier value might derive from its anatomical characteristics, i.e., the
3 parent artery that was fixed tightly to the skull base dura and the aneurysm itself was fixed, possibly
4 only partially, to a bony structure such as the anterior clinoid process, possibly producing unique
5 hemodynamic characters. To resolve these matters, we should perform subgroup analysis based on
6 its location after accumulating a sufficient number of cases and re-consider the significance of this
7 outlier value.

8 Third, from the point of view of the resolution of TOF-MRA, the image resolution of 1.5T TOF-
9 MRA was inferior to that of 3.0T TOF-MRA. Fortunately, we did not encounter any problems in
10 solving the images even using 1.5T TOF-MRA. We should precisely discriminate these two
11 different conditions because the results from two images might give potential differences that were
12 not detected in the present study.

13 Finally, we could not determine the relationship between the areas of temporally increased WSS
14 on the aneurysm dome and the actually enlarged regions because we could not detect them by
15 TOF-MRA images before and after aneurysm growth. Further analyses applied to more cases with
16 AN2WER using the high-resolution 3T-MRI may clarify this matter. In addition, we did not

validate the results histopathologically by comparing the aneurysm specimens taken from the actual surgery. Combined with histopathological analyses, the actual mechanisms contributing to aneurysm growth could be clarified.

CONCLUSION

Our newly developed CFD method enabled us to perform CFD analysis using TOF-MRA images alone, a task that cannot yet be performed with commercially available software. We conducted a retrospective analysis of the original aneurysm data before growth and demonstrated the actual hemodynamic situation in growing aneurysms.

Although further analysis of accumulated cases is needed to clarify obtained results, our present preliminary study demonstrated that transient, focal high WSS areas of the aneurysm sac at the peak systolic phase in the vicinity of constant low WSS areas might be related to future aneurysm growth.

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3

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5

FIGURE LEGENDS

Fig. 1. Reconstruction of blood vessel shape using TOF-MRA data

(A) Original TOF-MRA image, (B) blood vessel model extracted from the TOF-MRA image, (C) STL (stereolithographic) mesh data of the blood vessel model, (D) signed-distance function representing blood vessel walls (the contour plots represent each iso-surface of the signed-distance function, whose magnitude is the distance from the blood vessel wall, while the sign of the function is determined in order to distinguish the solid phase [wall] from the fluid phase [blood]), and (E) time variation of inlet velocity during one cardiac cycle. The boundary condition at the wall in lattice Boltzmann simulations is given by making use of the distance function.

(TOF-MRA, time-of-flight magnetic resonance angiography.)

Fig. 2. Illustrative case: Case 1, 69-year-old woman, right IC-Pcom AN

The aneurysm measured 8.5 mm before growth (first row) and enlarged to 11.8 mm (second row) in 11 months. TOF-MRA imaging (first column) and analysis of flow dynamics, including the streamline (second column), wall shear stress (WSS, third and fourth columns), and oscillatory shear index (OSI, fifth column) were successfully obtained. WSS 2 shows a back view of WSS 1.

WSS was focally increased at the aneurysm wall (red arrow).

The change in WSS during one cardiac cycle is shown in the third and fourth rows (the third shows the status before aneurysm growth, and the fourth shows the status after growth). At the peak systolic phase, WSS was elevated at the focal aneurysmal sac before growth (red arrow heads), where the aneurysm would later enlarge.

(IC-Pcom AN, Internal carotid- posterior communicating artery aneurysm; TOF-MRA, time-of-flight magnetic resonance angiography.)

Fig. 3. Visual comparison of WSS analyzed by AN2WER (upper row) and by Hemoscope Ver. 1.5 (lower row) in three cases (one per column)

The areas with low WSS (blue) and relatively high WSS (green) on the aneurysm sacs were almost matched between the two methods. The color distributions at the parent artery were also similar between cases 2 and 3.

(CFD, computational fluid dynamics; WSS, wall shear stress)

Fig. 4. Results of the growing group

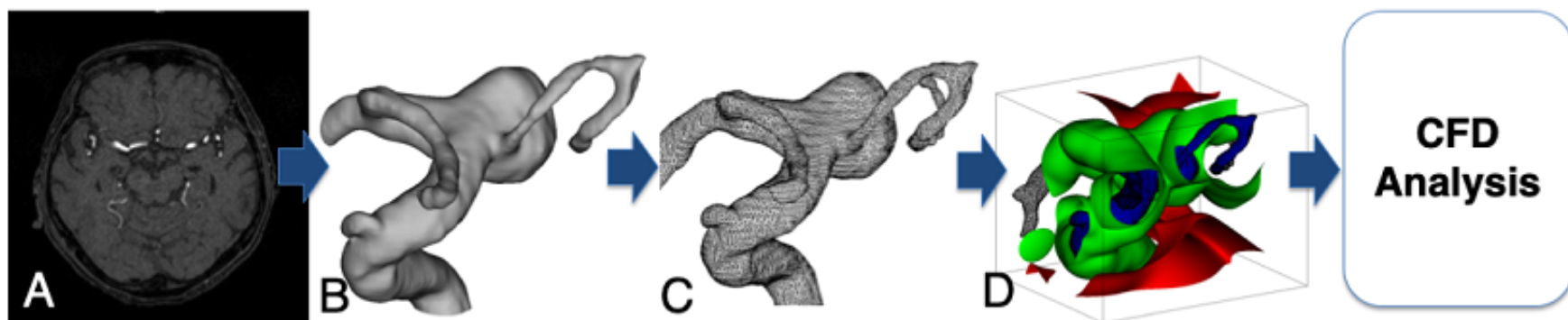
1 TOF-MRA images taken before and after aneurysm growth (first and second row, respectively).
2 The peak values of WSS maps were recognized at the peak systolic phase (third row). WSS was
3 focally increased on the walls of all aneurysms (red arrow). The mean values were 0.074, 0.106,
4 0.37, 0.13, 0.26, and 0.25 in cases 1 to 6, respectively. Fourth row: surface-rendered images
5 demonstrating the calculated five points of peak WSS (white cross marks)
6 (first column, case 2; second column, case 3; third column case 4; fourth column, case 5; fifth
7 column, case 6; sixth column, case 7).
8 WSS values are mean values at all five white cross marks in surface rendered images
9 (TOF-MRA, time-of-flight magnetic resonance angiography; WSS, wall shear stress)

10

11 Fig. 5. Results of the stable group

12 TOF-MRA images (first row), WSS map (second row) and surface-rendered images (third row) at
13 the peak systolic phase of the stable aneurysms. In cases 1, 3 and 5, no apparent increases in WSS
14 were recognized on the aneurysm sac. Obtained values were 0.0066, 0.045, and 0.0019,
15 respectively. In the remaining three stable aneurysms (cases 2, 4, and 6), focal increases of WSS
16 at the peak systolic phase (red arrow) were demonstrated. Obtained values were 0.487, 0.073, and

1 0.117, respectively (first column, case 1; second column, case 2; third column, case 3; fourth
2 column, case 4; fifth column, case 5; sixth column, case 6).
3 WSS values are the mean values at all five white cross marks in surface-rendered images
4 (TOF-MRA, time-of-flight magnetic resonance angiography; WSS, wall shear stress)
5
6 Fig. 6. Peak values of WSS on the focal aneurysm sac in both growing and stable aneurysms
7 The difference was statistically significant between the groups (* $p < 0.05$).
8 (ANs, aneurysms)

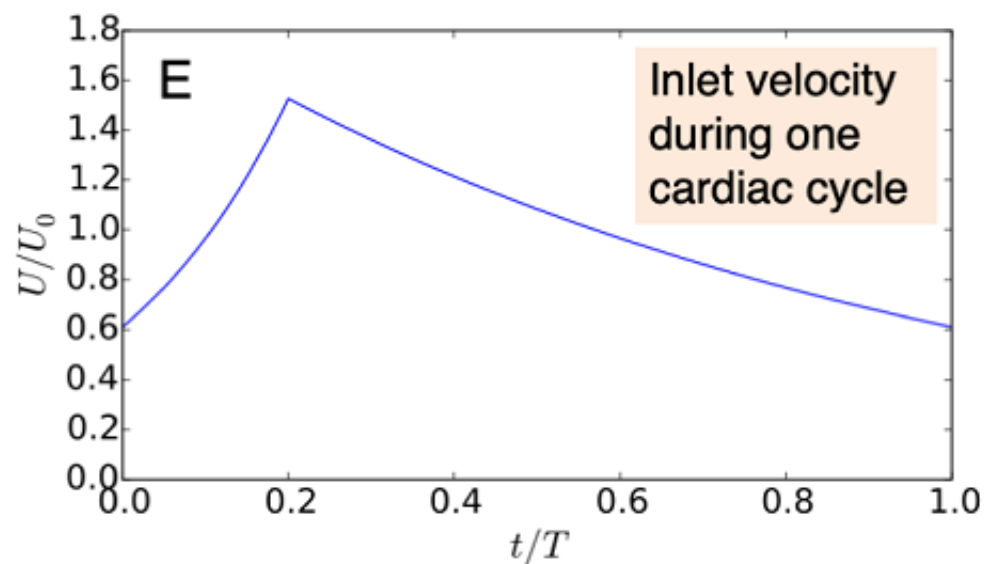


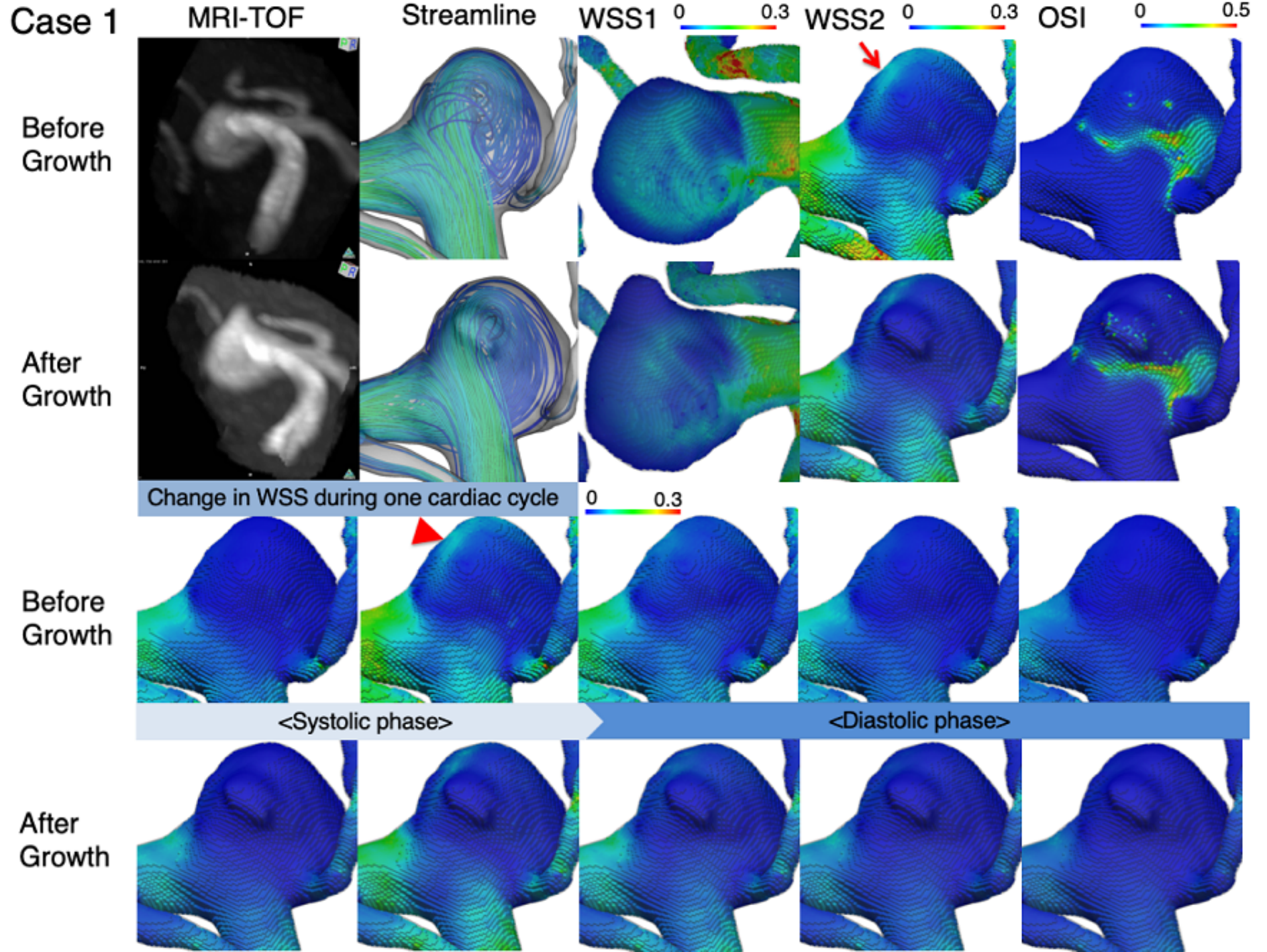
Dimensionless groups

Reynolds number 200

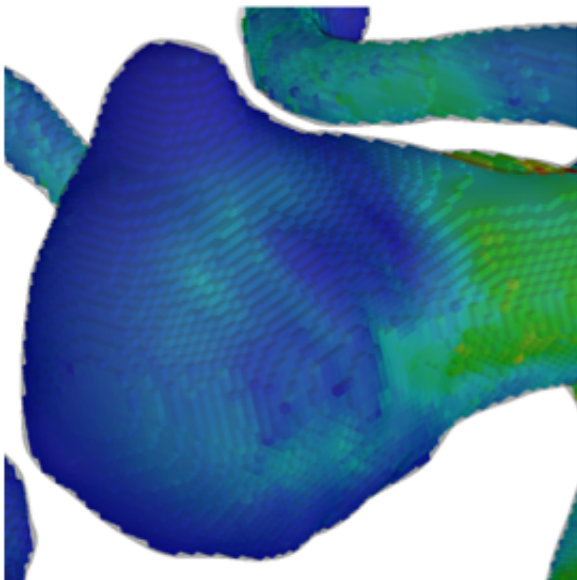
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Bingham number 0.1

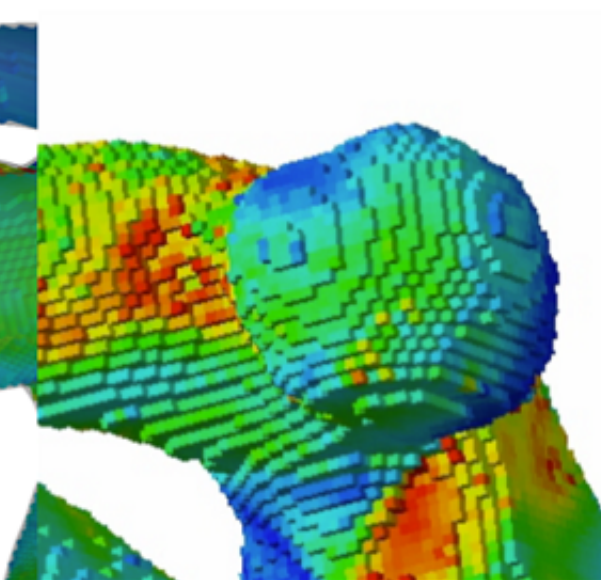




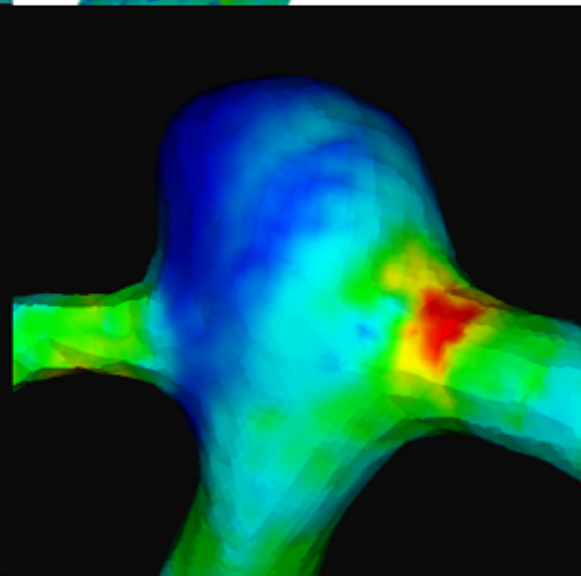
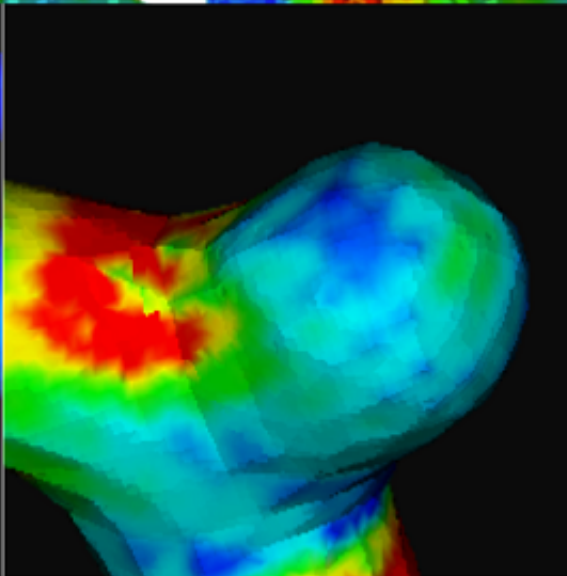
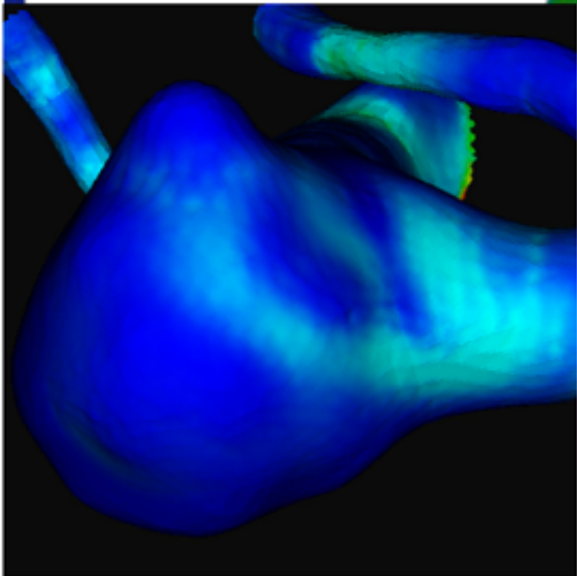
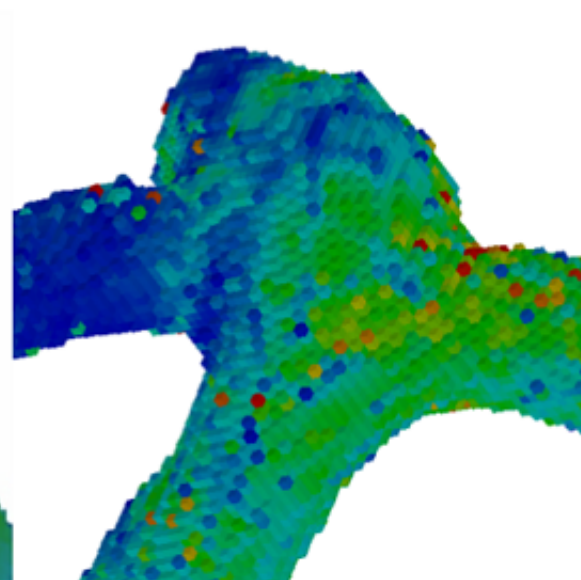
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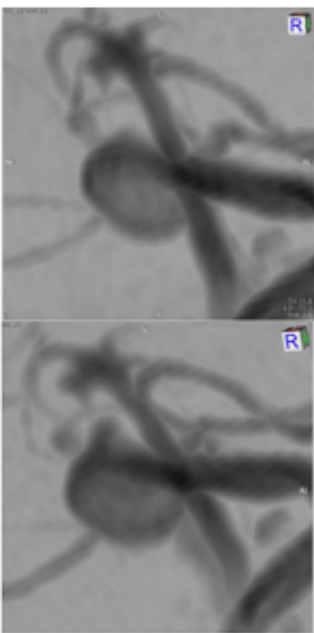
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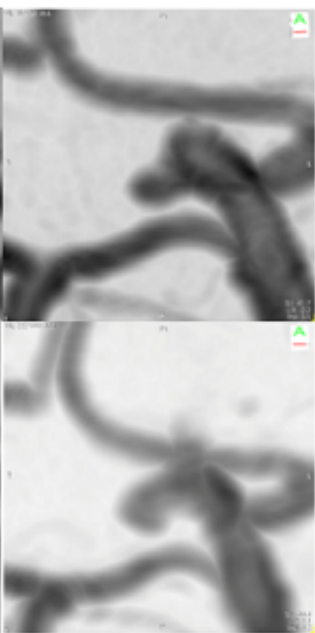
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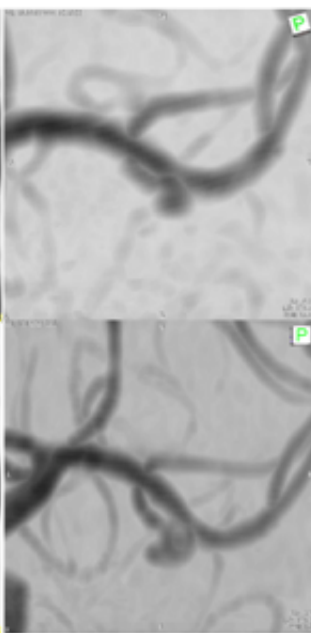
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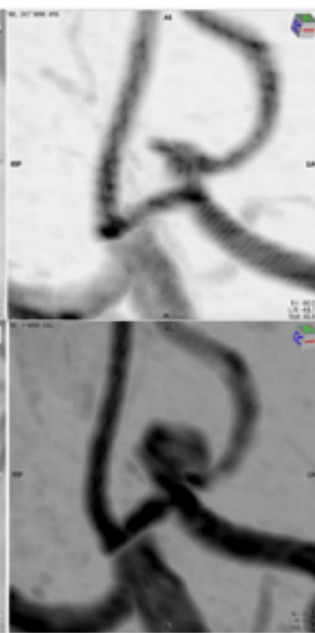
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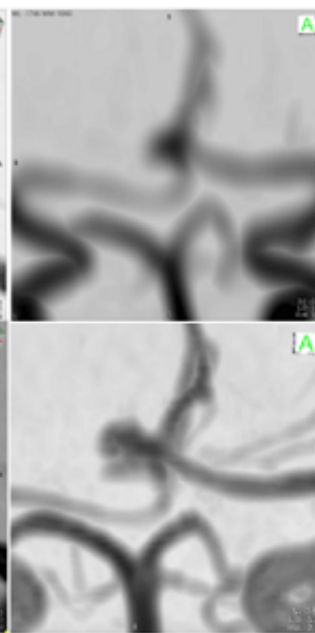
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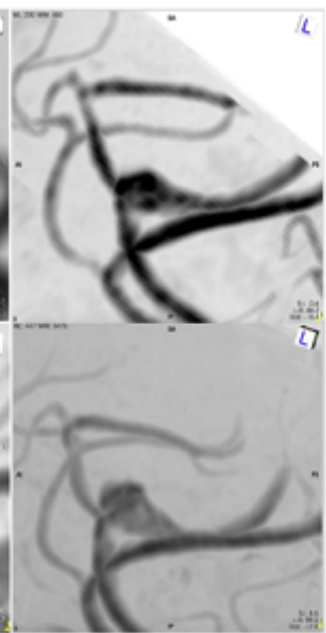
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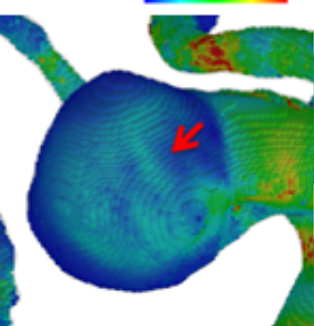
Case 5



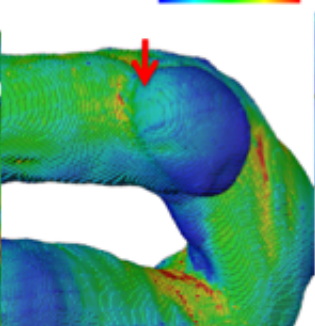
Case 6



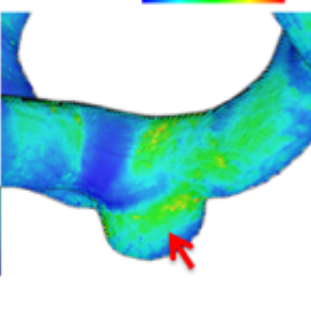
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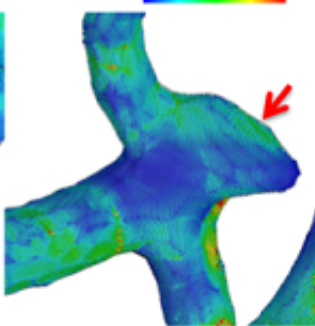
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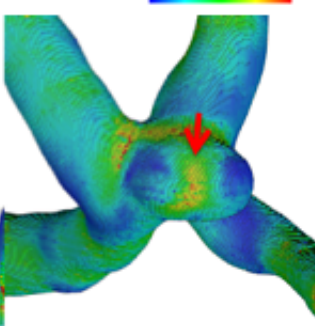
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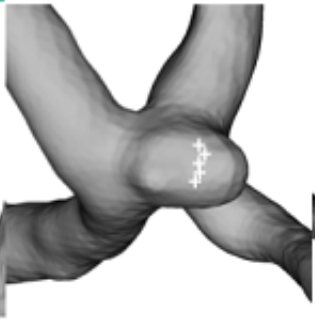
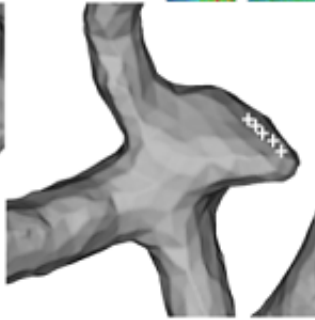
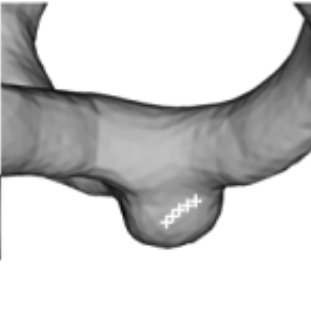
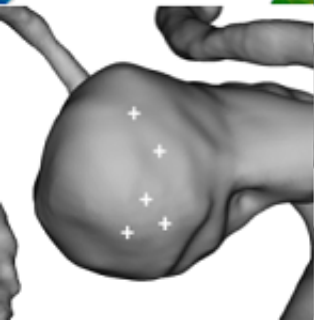
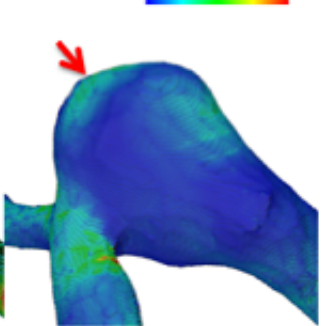
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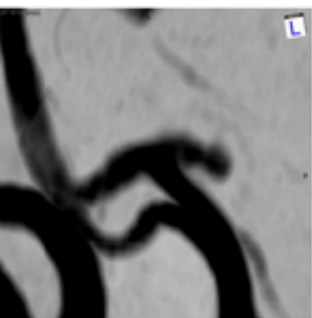
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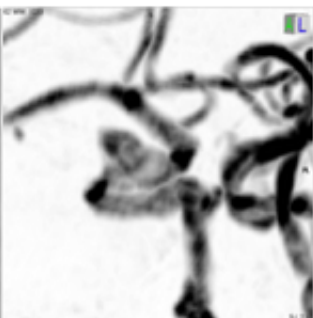
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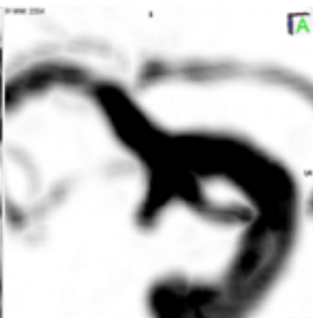
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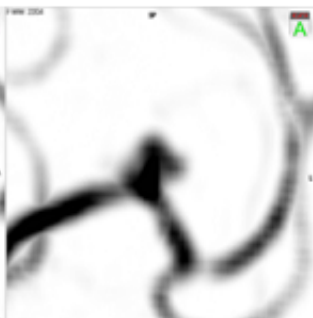
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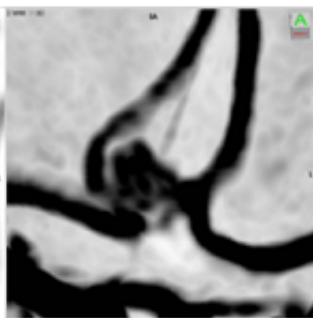
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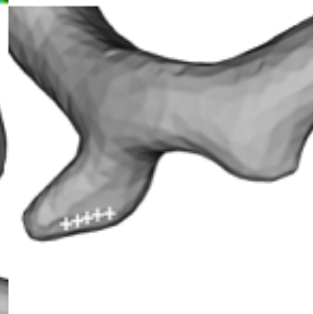
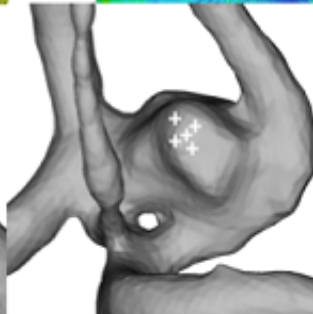
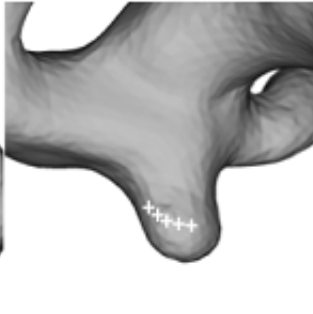
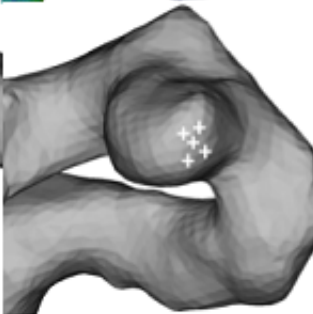
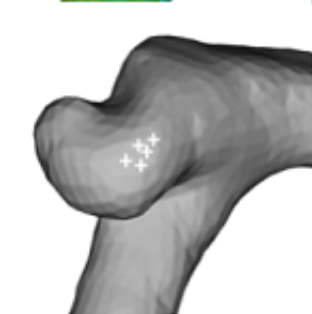
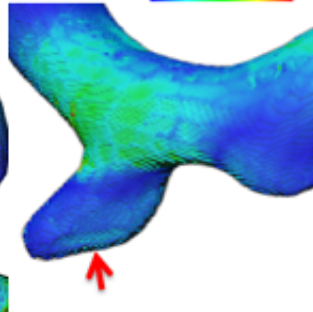
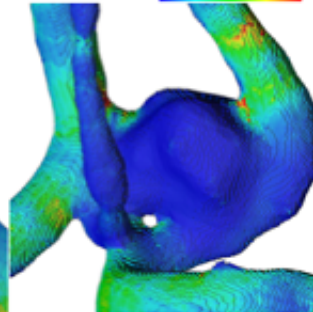
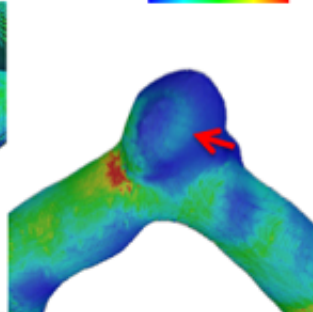
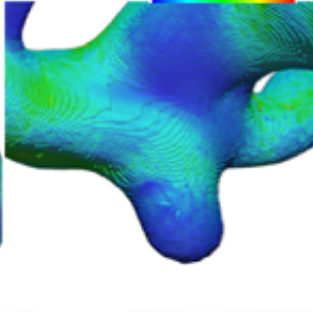
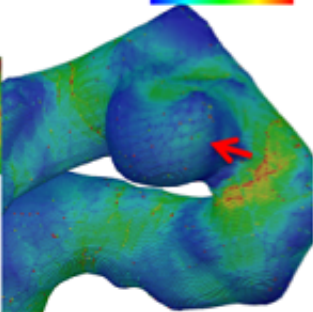
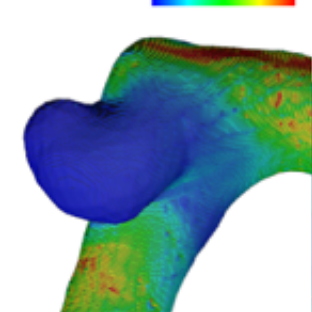
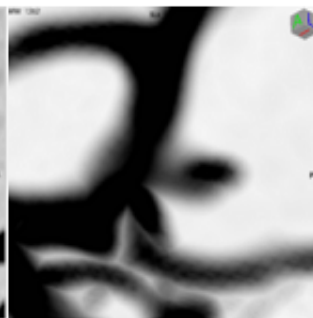
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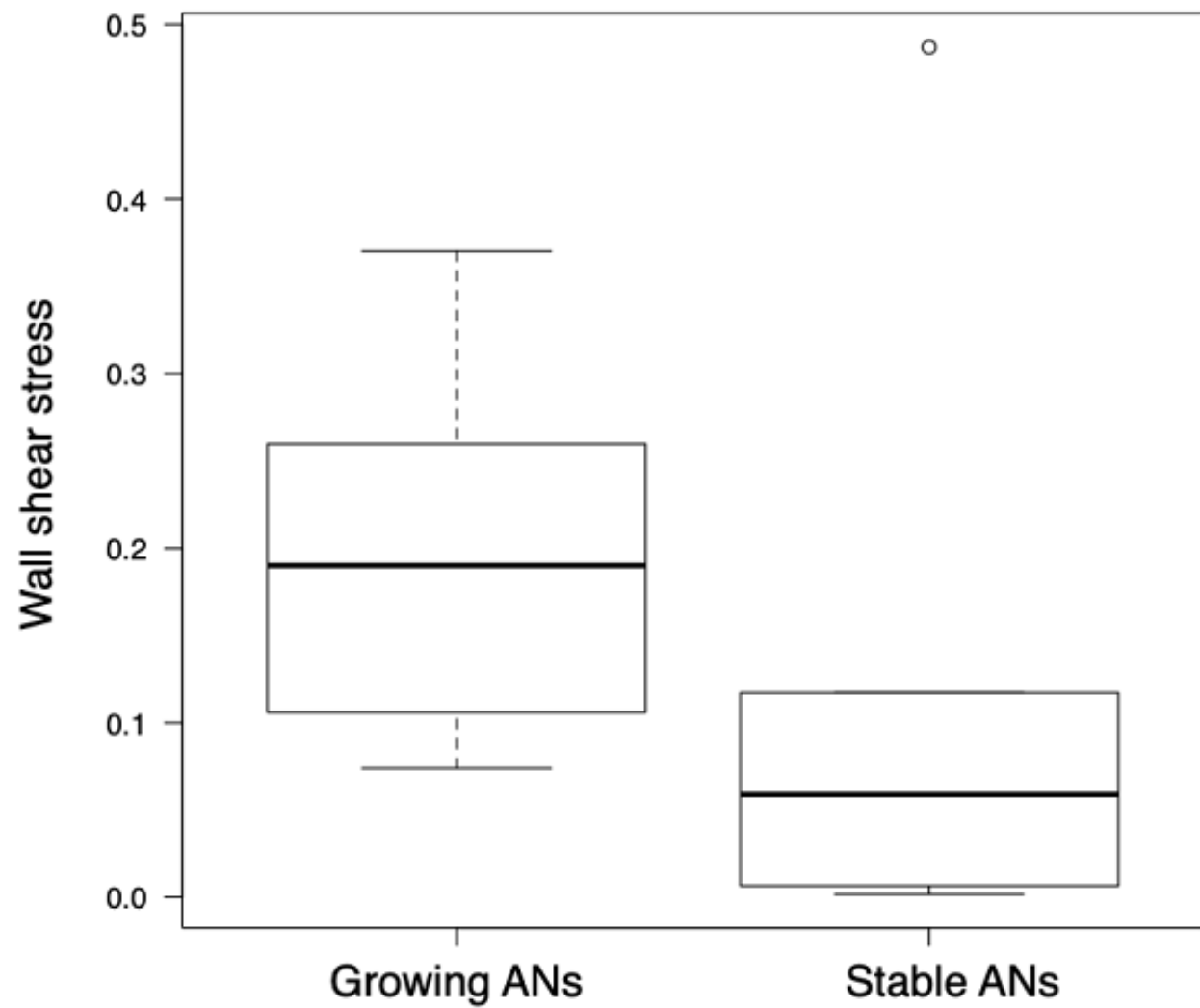


Case 5



Case 6





	Growing (n=6)	Stable (n=6)	p value
Mean age (years)	63.0±14.1	73.7±9.3	0.19
Men/women	1/5	1/5	1
Location			
IC	2 (33%)	3 (50%)	
Acom AN	2 (33%)	1 (17%)	
MCA	1 (17%)	1 (17%)	
VA-BA	0 (0%)	1 (17%)	
Distal ACA	1 (17%)	0	
F/U periods (month)	44.6	76.3	0.05
initial size	4.1±2.0	6.9±3.2	0.20
last size	6.1±2.6	–	