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Silicon-coated gold nano diffraction grating structures as plasmonic absorber for short wavelength infrared light

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Abstract: As a plasmonic absorber for short-wavelength infrared hyperspectral imaging, a silicon-coated gold nano diffraction grating structure is proposed. This plasmonic absorber leads to absorption peaks in short-wavelength infrared region by high refractive index of silicon coating on gold grating. It is relatively easy to be fabricated with smaller size than those of already known absorbers. By performing fabrication, simulation, and measurement, we demonstrate the sharp absorption peaks of short-wavelength infrared light using only 400–1000 nm grating interval. We believe this miniaturized absorber will enable to be applied to hyperspectral imaging without a spectroscope owing to its sharp absorption peak at a specific wavelength.

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1. Introduction

In recent years, demand for non-destructive and non-contact inspections using short-wavelength infrared (SWIR, wavelength range: 1–3 μm) spectroscopy has increased. SWIR light is highly transparent to substances such as package films and liquids, as well as unique absorption characteristics to water. Water absorbs only specific wavelength light (1450–1500 nm) in contrast to other wavelengths. Therefore, changes in the amount of water generated due to spoilage inside food can be detected easily. SWIR spectroscopy is used in various applications, such as medicine inspections [1], medical diagnoses [2, 3], and food inspections [4-7]. However, the currently marketed SWIR detectors require optical equipment such as a diffraction grating spectroscope for hyperspectral imaging [8, 9]. The additional equipment results in high cost and large device size, as well as considerable detection noise due to radiant heat from optical components [10]. Therefore, absorbers with wavelength dependence in the SWIR wavelength range of detectors are expected to enable hyperspectral imaging without requiring diffraction grating spectroscopy. By integrating the structures of SWIR detectors and absorbers with various absorption peak wavelengths as one imaging pixel, various wavelength bands can be detected instantly without using the conventional diffraction grating spectroscope. Various studies regarding wavelength-dependent plasmonic absorbers have been reported [11, 12], where metal nanostructures such as nanorods [13, 14], nanofins [15-17], metal-insulator-metal (MIM) [18] and grating structures [19-21] for bio-chemical or microelectromechanical system (MEMS) optical sensors [21-25] have been reported. However, a full width at half maximum (FWHM) of the structures proposed in Ref. [14] is about 170 nm. Therefore, it is challenging to obtain a narrow-band absorption peak using nanorods. Nanofins are challenging to fabricate because of their high-aspect-ratio nanostructures, which result in low structural controllability. Because MIM structures control the absorption wavelength based on the thickness of the insulator thin film, it is difficult to fabricate multiple absorbers with different film thicknesses on a same substrate to yield different absorption peak wavelengths for sensor applications. Grating structures have been used as spectroscopic elements because they can

46 yield a narrow band absorption peak and good controllability for absorption peak wavelengths
 47 by changing the grating interval. The interval required for SWIR absorption is similar to the
 48 wavelength, as described in Section 2. Thus, absorber miniaturization for high-spatial-
 49 resolution hyperspectral imaging is restricted. Hence, we focus on miniaturized SWIR
 50 absorbers with a narrow band absorption peak with a FWHM of less than 100 nm in the
 51 wavelength ranged from 1000 to 2000 nm (generally used for food inspection), excellent
 52 controllability, and a wide control wavelength range on the same substrate.

53 Herein, we propose silicon (Si)-coated gold (Au) nano diffraction grating structures, which
 54 are relatively easy to fabricate because of the excellent compatibility of these materials in
 55 nano/microscale MEMS fabrication. The optical characteristics of grating structures are
 56 significantly affected by a refractive index (dielectric index) of the surroundings. Therefore, by
 57 coating the grating structures with Si, it is expected to reduce the grating interval, thereby
 58 resulting in a high refractive index and an excellent integration with MEMS.

59 In this study, we fabricated, simulated, and measured Si-coated Au nano diffraction grating
 60 structures. The effects of the Si coating thickness and the height, grating interval, and width of
 61 the Au nano diffraction grating structures on the optical characteristics are reported herein.

62 2. Principle of NIR absorption

63 Propagating electromagnetic waves combine with the collective vibration of free electrons at
 64 the interface between a metal and dielectric under certain conditions in the resonance state [26-
 65 29]. This phenomenon is known as surface plasmon polariton (SPP), and its behavior can be
 66 derived from Maxwell's equations. In this phenomenon, surface plasmon wave (SPW)
 67 propagates along the interface between the dielectric and metal. The SPW wavenumber (k_{sp})
 68 is expressed as follows:

$$k_{sp} = \pm \frac{2\pi}{\lambda} \operatorname{Re} \left(\sqrt{\frac{\varepsilon_s \varepsilon_m}{\varepsilon_s + \varepsilon_m}} \right), \quad (1)$$

69 where λ , ε_s , and ε_m denote the wavelength of light in vacuum, permittivity of dielectric, and
 70 complex permittivity of the metal, respectively.

71 The horizontal component of the diffracted light at an incidence angle θ (k_x) is expressed
 72 as follows:

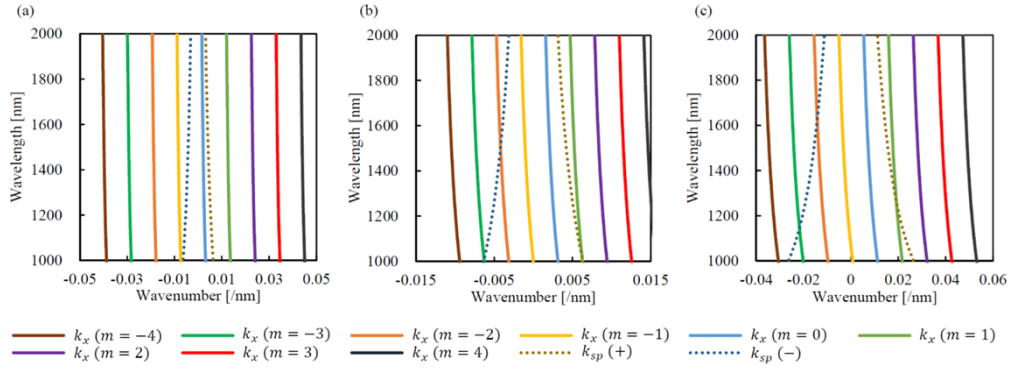
$$k_x = \frac{2\pi}{\lambda} \sqrt{\varepsilon_s} \sin \theta + \frac{2m\pi}{d}, \quad (2)$$

73 where m and d denote the diffraction mode with a positive or negative integer and a grating
 74 interval, respectively. SPP is generated when k_{sp} and k_x match, and SPP can be observed at
 75 the wavelength intersecting k_{sp} and k_x . To satisfy the resonance condition, a metal whose real
 76 part of the refractive index is negative must be used. Gold, silver, and aluminum are typically
 77 used in wavelength regions of visible light and longer [30]. We used Au because it is highly
 78 compatible with MEMS and less likely to cause surface oxidation.

79 When we consider a simple case in which light is incident on an Au plane, k_x contains no
 80 second term. Consequently, no intersections exist and hence no SPP generation. Although a
 81 method using a prism as a medium is easy and often used to match k_{sp} and k_x , it prevents the
 82 miniaturization of sensors. Therefore, absorbers with metal diffraction grating structures were
 83 used in this study. The resonance wavenumber (or wavelength) and the electromagnetic
 84 intensity are affected by d and θ . As an example, their relationships when using Au diffraction
 85 gratings with $d = 600$ nm and $d = 2000$ nm are shown in Figs. 1(a) and (b), respectively. x
 86 and y axes mean the wavenumber and the wavelength of k_{sp} and k_x , respectively. In this study,
 87 the target wavelength ranged from 1000 to 2000 nm. The angle of incidence was fixed at $\theta =$
 88 30° because of the specifications of the measuring equipment used in this study, as described

89 in Section 3. In the case of $d = 600$ nm, as shown in Fig. 1(a), no intersections were observed
 90 in the target wavelength range. By contrast, in the case of $d = 2000$ nm, as shown in Fig. 1(b),
 91 intersections were observed at wavelengths of 1506, 1021, and 1007 nm. Therefore, by
 92 selecting the appropriate d and θ , SPP is generated by simply injecting light without an
 93 additional optical system, such as a prism, because of the intersection. In this regard, several
 94 studies pertaining to the control of the absorption wavelength by changing d or θ have been
 95 reported [31, 32].

96 However, because a sufficient number of diffraction gratings is required to generate SPPs,
 97 it is difficult to reduce the size of an absorber with $d = 2000$ nm. Therefore, we propose Si-
 98 coated Au nano diffraction grating structures. The relationship between k_{sp} and k_x at $d = 600$
 99 nm is shown in Fig. 1(c). We can confirm that intersection wavelengths of 1628, 1263, and
 100 1146 nm were observed; in other words, SPP is generated in the SWIR region. In the cases
 101 shown in Figs. 1(a) and (b), the SPW propagates at the interface between vacuum (or
 102 atmosphere) and Au. By coating Si (which has a dielectric constant of 11.8–12.8 and a
 103 refractive index of 3.44–3.58 in the SWIR region) on the Au diffraction gratings, the SPW
 104 propagates between Au and Si, and the absorption wavelength can be controlled. Therefore, we
 105 assume that SPPs can be generated in the SWIR region even at a smaller grating interval of
 106 approximately 30% or less owing to the refractive index of Si. This is expected to contribute to
 107 the further miniaturization of SWIR sensors.
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Fig. 1. Calculated relationship between resonance wavelength and wavenumber of SPW wavenumber k_{sp} and horizontal component of diffracted light k_x at wavelength ranging from 1000 to 2000 nm. x and y axis mean the wavenumber and the wavelength of k_{sp} and k_x , respectively. Angle of incidence fixed at $\theta = 30^\circ$. Relationship when using Au diffraction gratings with (a) $d = 600$ nm, (b) $d = 2000$ nm (both without Si coating), and (c) $d = 600$ nm (with Si coating).

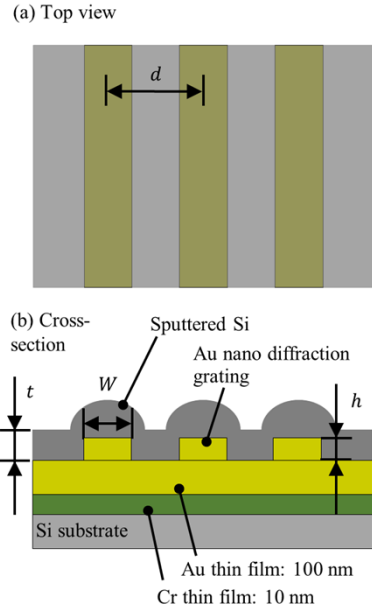
117 3. Methods

118 3.1 Structure

119 Figure 2 shows a schematic image and parameters of the Si-coated Au nano diffraction grating
 120 structures. The cross-sectional structures of the Au gratings and the coated Si depend on the
 121 fabrication process. We carried out the preliminary fabrication experiments to obtain the
 122 resulting structure and the available structural dimensions. In Section 3.1, the fabrication
 123 process, the fabrication result, and the parameters for simulations and experiments were
 124 presented.

125 For the diffraction grating structures, line and space patterns with length of $20 \mu\text{m}$ were
 126 fabricated on a Au thin film. First, a 10-nm-thick Cr thin film and a 100-nm-thick Au thin film
 127 were sequentially deposited on a bulk Si wafer using electron beam (EB) vapor deposition

128 equipment. Next, diluted positive resist ZEP 520A (Nippon Zeon) was spin coated onto the Au
 129 layer for EB lithography, followed by pre-baking on a hot plate. Subsequently, EB lithography
 130 of the Au nano diffraction grating patterns was performed. Subsequently, Au vacuum
 131 deposition and subsequent lift-off were performed to fabricate the Au nano diffraction gratings.
 132 Finally, Si was deposited via sputtering.
 133



134 Fig. 2. Schematic illustration and parameters of Si-coated Au nano diffraction grating structures.
 135 Au line and space patterns with $20\ \mu\text{m}$ length are fabricated on Au thin film and then Si is
 136 deposited.
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139 Figure 3 shows scanning electron microscopy (SEM) images of the fabricated Si-coated Au
 140 nano diffraction grating structures. Figures 3(a) and (b) show the Au nano diffraction gratings
 141 before they were coated with Si. Figures 3(c) and (d) show the cross-sectional images. The
 142 cross-sectional shape of the nano diffraction gratings was trapezoidal. The coating Si was
 143 complicated structure that covered the nano diffraction gratings and contained dents. The
 144 measured average values of the Si coating thickness (t), grating height (h), grating interval (d),
 145 and grating width (W) of the Si-coated Au nano diffraction grating structures are shown in
 146 Table 1. t was controlled by sputtering time for absorption peaks in the SWIR region. These
 147 were determined as a parameter for simulations and experiments.
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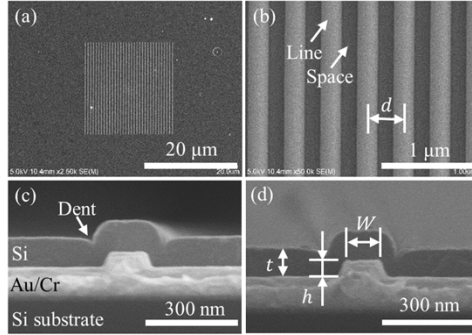


Fig. 3. SEM images of fabricated Si-coated Au nano diffraction grating structures, which are fabricated on Au thin film via EB lithography, Au vapor deposition, and Si sputtering. (a), (b) show top view of Au nano diffraction gratings prior to coating Si. (c), (d) show cross-sectional images of Au nano diffraction gratings after coating Si.

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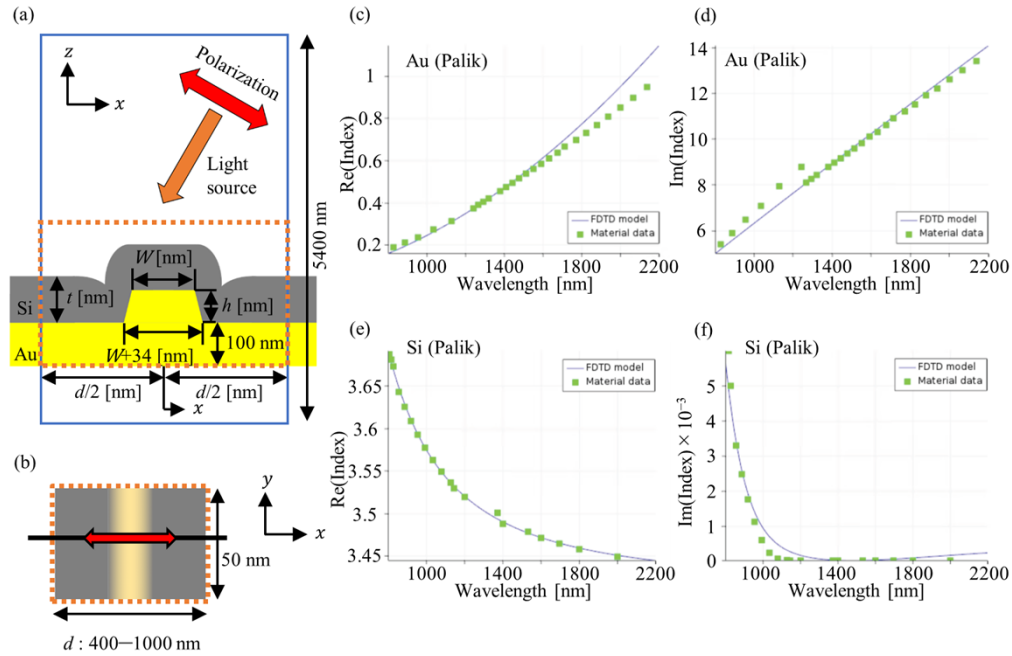
Table 1. Average values of measured grating height (h), thickness of Si coating (t), grating interval (d), and grating width (W) of Au nano diffraction grating structures

Dimension parameters	Design [nm]
Grating height (h)	40
Si coating thickness (t) (Sputtering time [min])	0, 77, 93, 102, 119 (0, 12.5, 15.0, 17.5, 20.0)
Grating interval (d)	400, 500, 600, 700, 800, 900, 1000
Grating width (W)	23, 45, 69, 101, 121, 141, 170, 202

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158 3.2 Modeling

159 As a finite differential time domain (FDTD) method, we used FDTD Solutions (Lumerical),
160 which is commercially available simulation software. The simulation model shown in Fig. 4
161 was designed based on the dimensions and shapes obtained from the SEM images. In
162 measurement, angle of light θ through the reflective objective lens irradiating the absorber
163 ranged from 16° to 45° . Therefore, we set $\theta = 30^\circ$ because the median value had peak intensity.
164 We applied the broadband fixed angle source technique (BFAST) to the light source, which is
165 a plane wave and can calibrate different incident angles for each wavelength. The BFAST is
166 effective when using an angled light source in a periodic structure. For the periodic boundary
167 condition, we used the BFAST symmetric boundary condition to shorten the simulation time
168 for the x - and y -planes. The perfectly matched layer absorption boundary condition was used
169 for the z -plane. The width of the simulation area in the x -direction varied from 400 to 1000
170 nm, which corresponded to d . The length and height of the simulation area were set to 50 and
171 5400 nm, respectively, in the y - and z -directions. The data by Palik was used to set the complex
172 refractive index of Au and Si as shown in Figs. 4(c)-(f). The mesh size of the complicated
173 structures such as a dent or a corner was set to 3 nm. The mesh size was determined because
174 no significant effect was confirmed at 3 nm or less. The auto-meshing function of the FDTD
175 software was adapted to the other part. In the simulation, the absorption spectra of the Si-coated
176 Au nano-diffraction grating structures were calculated. We investigated the effects of h , t , d ,
177 and W on the absorption spectrum and absorption peak wavelengths. The reflection and
178 transmission spectra were calculated via FDTD simulation at wavelength of 1000–2000 nm,
179 and the absorption was calculated as $A = 100 - T - R$. In addition, the electric field intensity
180 distributions at the absorption peak wavelengths were evaluated.
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Fig. 4. Simulation model and complex refractive indices using FDTD Solutions (Lumerical); model is based on dimensions and shapes obtained from SEM image. Periodic boundary condition was used. (a) Sectional view. (b) Top view. (c)-(f) complex refractive indices of (c), (d) Au, and (e), (f) Si. Plots and solid lines indicate discrete material data and fitting result of refractive indices, respectively.

200 3.3 Measurement

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Absorption A [%] is expressed in terms of transmittance T [%] and reflectance R [%] as follows: $A = 100 - T - R$. In this study, the absorption spectra were calculated as $A = 100 - R$ because the transmission of the Au thin film was negligible since the thickness of the Au layer was 100 nm, which provided a low transmittance of 2% or less calculated by the simulation. The reflectance was measured using an ultraviolet–visible/near-infrared microspectrophotometer (MSV-5200DGK, JASCO). A Cassegrain-type reflective objective lens equipped with a microspectrophotometer was used. A plane Au sample without patterns was used as a reference for the reflection spectra. The wavelength range for measurement was set from 1000 to 2000 nm.

211 4. Results

212 4.1 Effects of Si coating and grating height (h)

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We investigated the effects of the grating height and Si coating using the FDTD simulation. Figure 5 shows the simulated absorption spectra at $t = 102$ nm, $d = 600$ nm, $W = 101$ nm, and $h = 30$ – 50 nm. At $h = 30$ nm, we observed four absorption peaks at wavelengths of 1674, 1452, 1242, and 1170 nm, although no absorption peaks were observed without Si coating, as shown in Fig. 5(i). The spectrum without a Si coating ($t = 0$ nm) shows the absorption of less than 4% without peaks. We found the Si coating contributed to the absorption of the SWIR light in simulation as mentioned in Sections 1 and 2. The above mentioned absorption peaks are referred to herein as the first, second, third, and fourth peaks, respectively. They are the ordinal numbers from longer wavelengths, and don't correspond to the diffraction mode shown

211 in Eq. (2) and Fig. 1. We discovered the absorption depended significantly on h . In particular,
212 no second peak was observed when $h = 40\text{--}50$ nm.

213 Figure 6 shows the electric field intensity distributions of each simulated absorption peak
214 wavelength for $h = 30$ nm. As shown in Figs. 6(c) and (d), the electric field at the corners of
215 the trapezoidal upper base of the Au nano diffraction gratings are enhanced, and the
216 electromagnetic waves propagate at the interface between Au and Si at wavelengths of 1242
217 nm (third) and 1170 nm (fourth). As shown in Figs. 6(a) and (b), the electric field strengthened
218 in the dented part of the Si-coated gratings at wavelengths of 1674 nm (first) and 1452 nm
219 (second). The first and second peaks indicated more significant effects by the dented part on
220 the peak height than the third and fourth peaks. The lower absorption peaks were assumed to
221 be due to the greater distance from the Au/Si interface to the dented part than to the Au corners,
222 which resulted in a lower electric field (Fig. 6) and a greater absorption height. The dented part
223 included significantly complicated structures, particularly in a narrow space.

224 Figure 7 shows the simulated and the experimentally measured absorption spectra of the
225 absorbers with $d = 600$ nm, $W = 101$ nm, and $t = 102$ nm or $t = 0$ nm (without a Si coating).
226 When $t = 0$ nm, an absorption of 5% or less without peaks at wavelengths from 1000 to 2000
227 nm was observed, whereas the absorber with a Si coating of $t = 102$ nm indicated large
228 absorption peaks at wavelengths of 1591, 1412, 1165, and 1100 nm. We also confirmed the Si
229 coating contributed to the absorption of the SWIR light in experiment. When $t = 0$ nm, neither
230 the simulated nor measured results indicated an absorption peak in the SWIR region. These
231 results are consistent with theory because the case does not involve any intersections in the
232 dispersion relation shown in Fig. 1(a). The second peak has a high absorption rate of 84.8%
233 and a narrow bandwidth with a FWHM of 78 nm in the SWIR region. This is well below about
234 100 nm of the absorbers reported in recent study [19].

235 In this paragraph, the simulated and the experimental results were compared. No second
236 peak was observed when $h = 40\text{--}50$ nm, and the absorption (peak heights) of the simulated
237 results for the first and second peaks were greatly different from those of the experimental
238 results. The experimentally measured absorption at the wavelength of 1412 nm (second) was
239 84.8%, whereas that of 1452 nm (second) was 12.5% in the simulation for $h = 30$ nm, which
240 was significantly less than the measured value. Owing to the complicated structures such as
241 dented part with narrow space, the accurate modeling for simulation is difficult; hence, the
242 experimental and simulated results for the absorption height differ. In addition, we considered
243 the complex refractive index of the sputtered Si differs from the Palik data used in this study
244 because the sputtered Si is thought to be amorphous [33]. However, the simulated results
245 exhibited the tendency of the experimental results for the peak wavelengths. The diffraction
246 gratings with $h = 30$ nm indicated four absorption peaks in simulation as well as the
247 experimental results. We confirmed that the absorption peak wavelengths of the simulated
248 results were similar to those of the experimental results, where it shifted to longer wavelength.
249 Hence, we used a model with $h = 30$ nm in the subsequent simulation to clarify the absorption
250 peaks.

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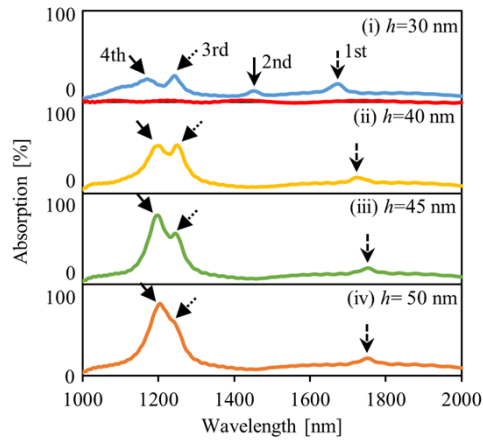


Fig. 5. Simulated absorption spectra of Si-coated Au nano diffraction grating absorbers with effect of height of nano diffraction gratings (h) for $t = 102$ nm, $d = 600$ nm, $W = 101$ nm, and $h = 30$ – 50 nm at wavelength ranging from 1000 to 2000 nm. In (i) $h = 30$ nm, spectrum for $t = 102$ nm (without a Si coating) is shown by red solid line.

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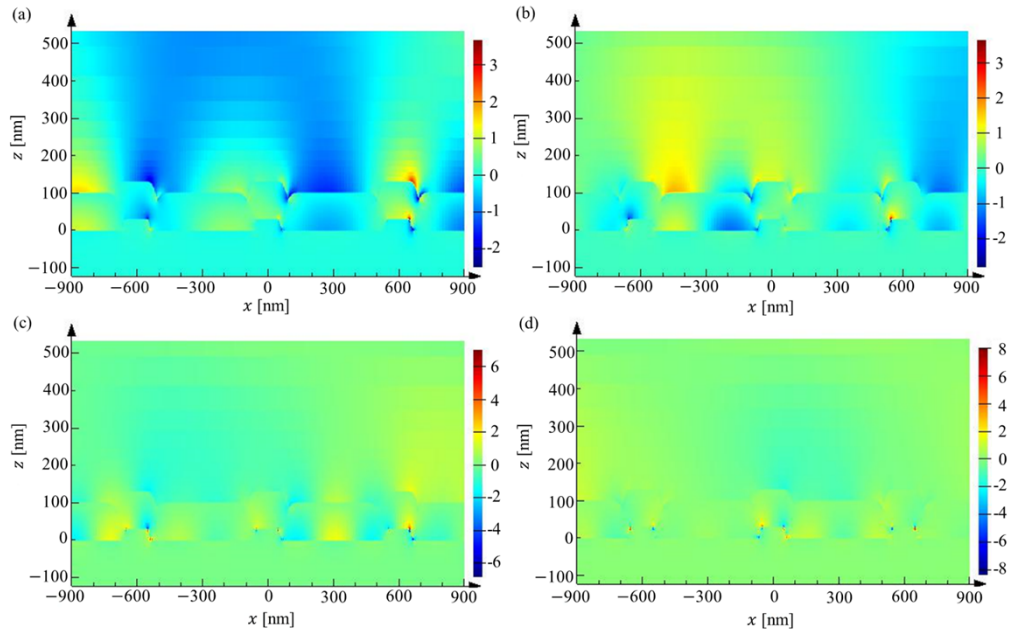


Fig. 6. Simulated electric field intensity distributions of each simulated absorption peak wavelengths of Si-coated Au nano diffraction grating absorbers for $t = 102$ nm, $d = 600$ nm, $W = 101$ nm, and $h = 30$ nm. (a) First peak at 1674 nm, (b) second peak at 1452 nm, (c) third peak at 1242 nm, and (d) fourth peak at 1170 nm.

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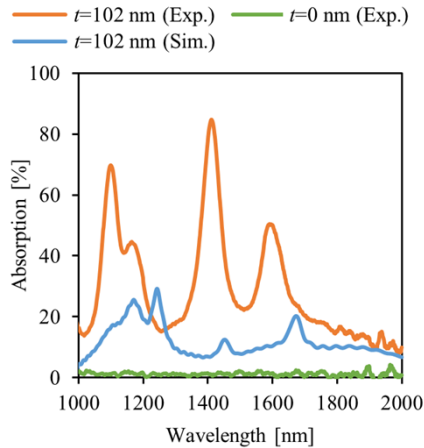


Fig. 7. Experimentally-measured (Exp.) and simulated (Sim.) absorption spectra of Si-coated Au nano diffraction grating absorbers for $d = 600$ nm, $W = 101$ nm, and $t = 102$ nm at wavelength ranging from 1000 to 2000 nm. Case of $t = 0$ nm (without a Si coating) is shown.

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270 4.2 Effect of Si coating thickness (t)

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Next, we investigated the effect of the Si coating thickness (t). Figures 8(a) and (b) show the simulated and experimentally-measured absorption spectra at $t = 0, 77, 93, 102,$ and 119 nm; $d = 600$ nm; and $W = 101$ nm, respectively. The absorption spectra for the case without Au nano diffraction gratings are also shown.

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In simulation, it was confirmed that the absorbers without grating structures indicated a slight change in the absorption wavelength depending on the Si coating thickness as shown in Fig. 8 (dotted lines); however, a clear absorption peak was not observed. On the other hands, the absorbers with grating structures showed clear absorption peaks. We confirmed the absorption peaks in SWIR region of 1000-2000 nm at t ranging from 77 to 119 nm used in this study. We found the absorption peak wavelengths shifted to longer as t increased focusing on the first and second peaks because these peaks were clearly observed without peak's superposition. The dependency of Si coating thickness is observed because the electric field of SPW goes out of the Si thin layer, ranging from 77 to 119 nm, as shown in Fig. 6.

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In measurement, when $t = 77$ nm, peak wavelengths were observed at 1387 nm (first), 1239 nm (second), 1081 nm (third), and 1009 nm (fourth). The peak wavelengths at $t = 77$ nm were shorter than those at $t = 93$ nm. When $t = 119$ nm, the absorption peaks appeared at 1694 nm (first), 1493 nm (second), 1196 nm (third), and 1123 nm (fourth). We found the four absorption peak wavelengths shifted to longer with increasing t as with the simulation. The wavelength of the second peak increased by 254 nm from 1239 to 1493 nm as t increased from 77 to 119 nm. The peak wavelengths can be controlled by changing t . The relationship between t and the absorption peak wavelengths is shown in Fig. 9. In both results, we confirmed the absorption peaks due to the Si coating, and the absorption peak wavelengths shifted to longer as t increased.

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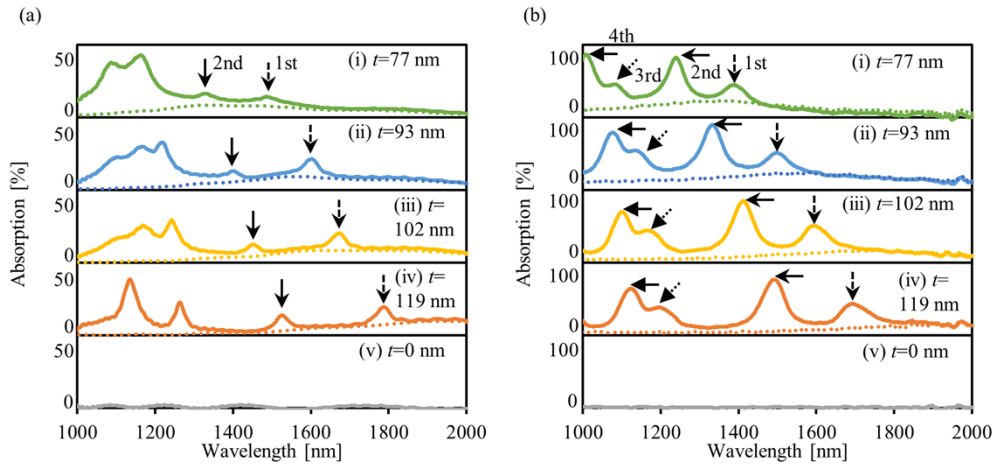


Fig. 8. Effect of Si coating thickness (t). (a) Simulated and (b) experimentally-measured spectra of Si-coated Au nano diffraction grating absorbers for $t =$ (i) 77, (ii) 93, (iii) 102, (iv) 119, (v) 0 nm; $d = 600$ nm; and $W = 101$ nm at wavelength ranging from 1000 to 2000 nm. Solid and dotted lines indicate spectra in cases with and without Au nano diffraction gratings, respectively. Absorption ranges of these spectral graph in simulation and experiment are set from 0 to 50% and from 0 to 100%, respectively.

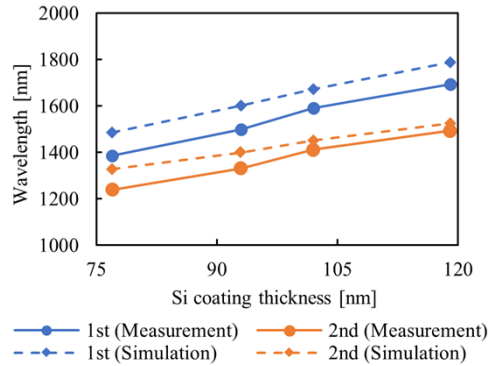


Fig. 9. Relationship between t and absorption peak wavelength ranging from 1000 to 2000 nm based on simulated and experimentally-measured results.

4.3 Effect of grating interval (d)

Next, we investigated the effect of the grating interval (d). Figures 10(a) and (b) show the simulated and experimentally-measured absorption spectra at $t = 102$ nm, $d = 400$ – 1000 nm, and $W = 101$ nm, respectively. The absorption spectrum for the case without Au nano diffraction gratings are also shown in (viii).

In simulation, we found the absorption peak wavelengths shifted to longer as d increased focusing on the first and second peaks. This tendency is consistent with the theory as mentioned in Section 2. With increasing d from 400 to 1000 nm, the first and second peaks were shifted from 1463 to 1961 nm, and from 1238 to 1679 nm, respectively.

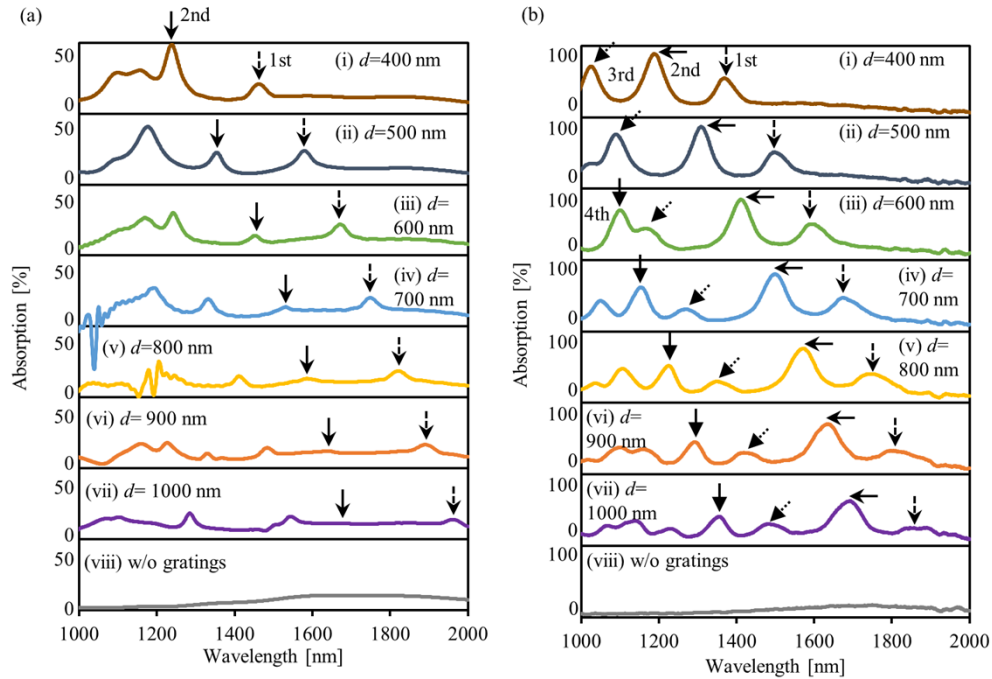
In measurement, when $d = 400$ nm, the peak wavelengths appeared at 1370 nm (first), 1189 nm (second), and 1025 nm (third). Fourth and higher wavelength peaks were not observed. The fourth and fifth peaks with small absorption appeared at $d = 600$ and 700 nm, respectively, when d increased. The peak wavelengths increased with d . When $d = 1000$ nm,

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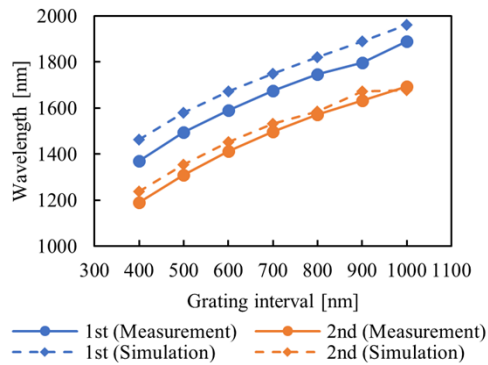
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321 the spectrum indicated absorption peaks at 1891 nm (first), 1693 nm (second), 1479 nm (third),
 322 and 1356 nm (fourth). At wavelengths shorter than the fourth peak, small absorption peaks
 323 appeared. The absorption peak wavelengths shifted to longer from 1189 to 1693 nm as d
 324 increased from 400 to 1000 nm, as indicated by the second peak, which demonstrated the
 325 highest absorption. The relationship between d and absorption peak wavelengths in simulation
 326 and experiment is shown in Fig. 11. From both results, we confirmed the absorption peak
 327 wavelengths shifted to longer as d increased, indicating good agreement between both results.
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 330 Fig. 10. Effect of grating interval (d). (a) Simulated and (b) experimentally-measured absorption
 331 spectra of Si-coated Au nano diffraction grating absorbers for $t = 102$ nm, $d = 400$ – 1000 nm
 332 ((i)–(vii)), and $W = 101$ nm at wavelengths ranging from 1000 to 2000 nm. Case without Au
 333 nano diffraction gratings is shown (viii). Absorption ranges of these spectral graph in simulation
 334 and experiment are set from 0 to 50% and from 0 to 100%, respectively.
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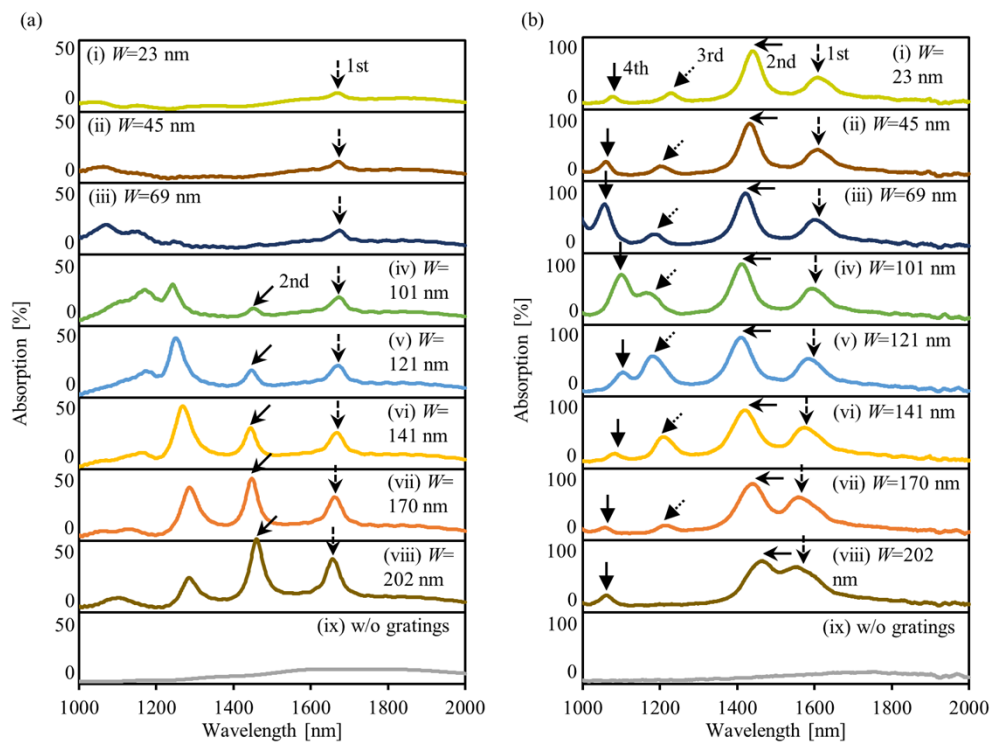


336
 337 Fig. 11. Relationship between d and absorption peak wavelength ranging from 1000 to 2000 nm
 338 based on simulated and experimentally-measured results.
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343 4.4 Effect of width of nano diffraction gratings (W)

344 Finally, we investigated the effect of the width of the nano diffraction gratings (W). Figures
345 12(a) and (b) show the simulated and experimentally-measured absorption spectra at $t = 102$
346 nm, $d = 600$ nm, and $W = 23$ – 202 nm, respectively. In simulation, the wavelengths of the first
347 and second peaks were independent of W ranging from 23 to 202 nm. This is because the width
348 does not affect the peak wavelengths, according to the theory. In measurement, when $W = 45$
349 nm, peak wavelengths were observed at 1610 nm (first), 1432 nm (second), 1200 nm (third),
350 and 1060 nm (fourth). When $W = 170$ nm, absorption peaks were observed at 1559 nm (first),
351 1438 nm (second), 1214 nm (third), and 1058 nm (fourth). The second peak wavelengths shifted
352 slightly to longer wavelengths, and the first peak shifted to shorter wavelengths as W increased.
353 The relationship between W and the absorption peak wavelengths in simulation and experiment
354 is shown in Fig. 13. The tendency of experiment are consistent with the simulation.
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Fig. 12. Effect of width of nano diffraction gratings (W). (a) Simulated and (b) experimentally-measured absorption spectra of Si-coated Au nano diffraction grating absorbers with effect of W for $t = 102$ nm, $d = 600$ nm, and $W = 23$ – 202 nm ((i)–(viii)) at wavelengths ranging from 1000 to 2000 nm. Case without Au nano diffraction gratings is shown in (ix). Absorption ranges of these spectral graph are set from 0 to 100% and from 0 to 50%, respectively.

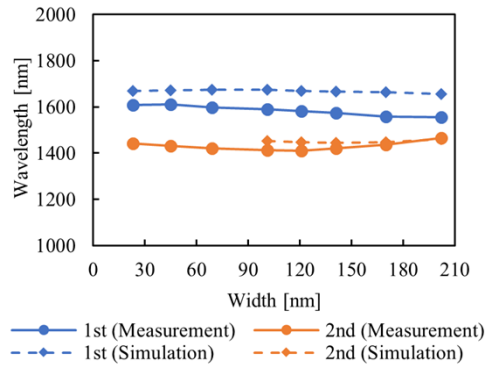


Fig. 13. Relationship between W and absorption peak wavelength ranging from 1000 to 2000 nm based on simulated and experimentally-measured results.

We discovered the effect of t or d prominent although that of W was less. By comparing between the simulated and experimentally-measured results, we confirmed that both indicated absorption peak wavelength shifts and hence validated the proposed structure. Furthermore, we demonstrated that coating the Au diffraction grating structures with Si reduced the grating interval. The grating interval of this proposed absorbers is 400-1000 nm for SWIR, which is much smaller than 1050-1350 nm of the absorbers reported in recent studies [19]. Therefore, we conclude that adopting the proposed absorber will result in the miniaturization of plasmonic optical sensors.

5. Conclusion

We herein propose Si-coated Au nano diffraction grating structures as miniaturized SWIR absorbers with a narrow band absorption peak, excellent controllability, and a wide control wavelength range on a same substrate. We performed nanofabrication, simulation using the FDTD method, and measurement for Si-coated Au nano diffraction grating structures. It was confirmed that Si coating contributed to the absorption of SWIR light at wavelength ranging from 1000 to 2000 nm owing to the high refractive index of Si. Three or four narrowband absorption peaks with a FWHM of approximately 75 nm were observed, and their maximum absorption was 86.6%. We found the absorption peak wavelengths shifted to longer as the Si coating thickness increased. Whereas the absorption peak wavelengths shifted to longer as the grating interval increased, a slight shift occurred owing to the grating width. We discovered that the grating interval and Si coating thickness effectively controlled the absorption peak wavelengths. Additionally, the required grating interval is 400-1000 nm, which is much smaller than those of the structures reported in recent studies. The experimental results exhibited the same tendency as the FDTD simulated results regarding the peak wavelengths. Therefore, we believe that this absorber will enable low-cost and miniaturized optical sensors leading to non-destructive and non-contact inspections without requiring a spectroscope.

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Data availability. Data underlying the results presented in this paper are not publicly available at this time but may be obtained from the authors upon reasonable request.

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